

# Today's outline - September 23, 2024





- Mirrors

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- Ideal refractive surface

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Reading Assignment: Chapter 4.1–4.2

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Homework Assignment #03:

Chapter 3: 1,3,4,6,8

due Monday, September 30, 2024

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Homework Assignment #03:  
Chapter 3: 1,3,4,6,8  
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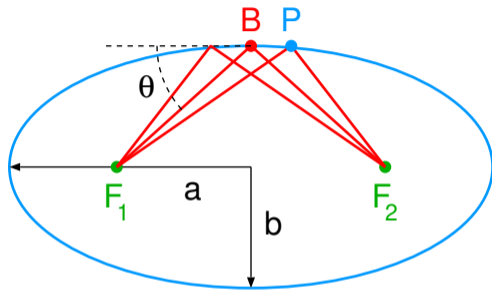
Homework Assignment #04:  
Chapter 4: 2,4,6,7,10  
due Monday, October 14, 2024



# Tangential focusing mirror



The shape of an ideal mirror is an ellipse, where any ray coming from one focus will be projected to the second focus.

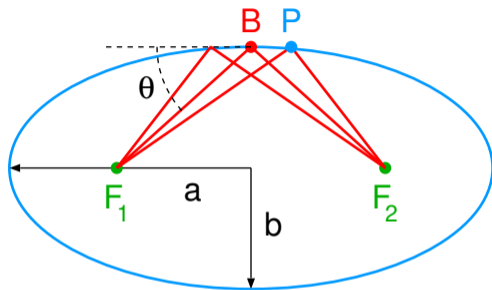


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$$F_1P + F_2P = 2a$$



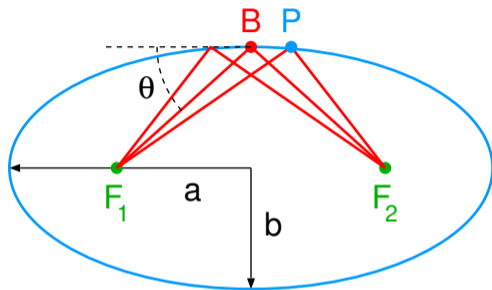
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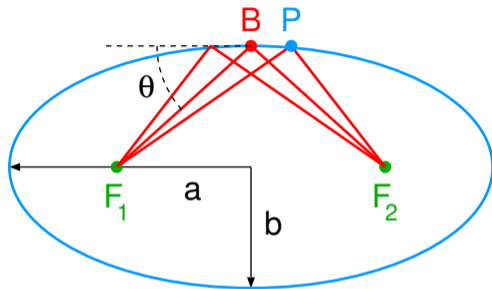
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$$\sin \theta = \frac{b}{a}$$

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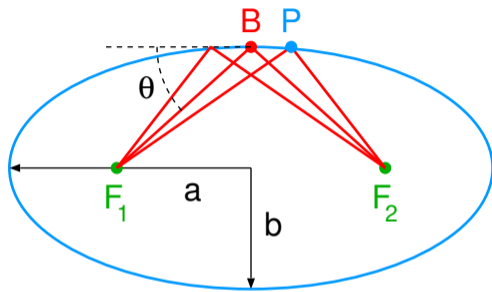


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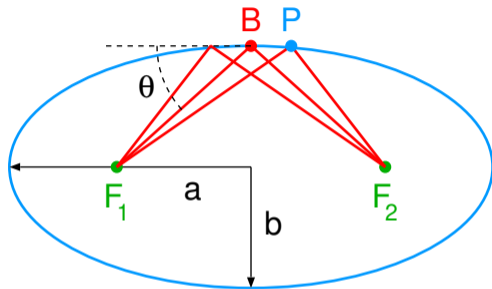


$$\frac{1}{f} = \frac{1}{o} + \frac{1}{i}$$

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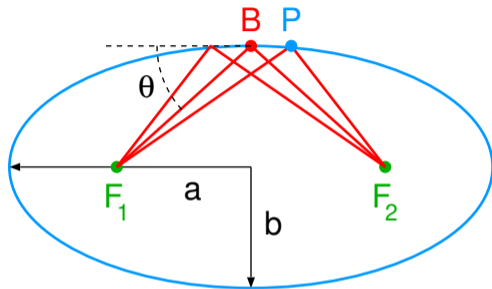
$$\frac{1}{f} = \frac{1}{o} + \frac{1}{i} = \frac{2}{a}$$

$$f = \frac{a}{2}$$

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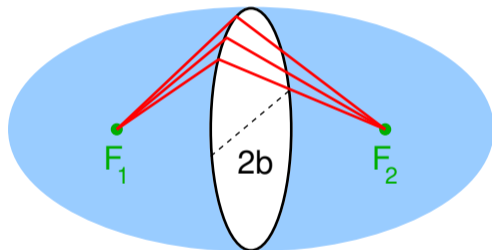
$$\frac{1}{f} = \frac{1}{o} + \frac{1}{i} = \frac{2}{a}$$

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## Saggital focusing mirror



Ellipses are hard figures to make, so usually, they are approximated by circles. In the case of saggital focusing, an ellipsoid of revolution with diameter  $2b$ , is used for focusing.



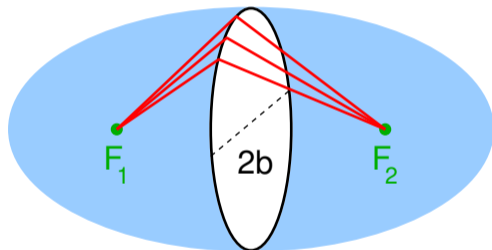


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$$\rho_{saggital} = b = 2f \sin \theta$$



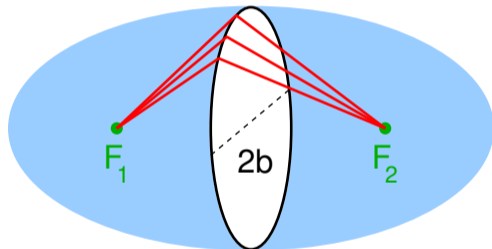
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The tangential focus is also usually approximated by a circular cross-section with radius



# Sagittal focusing mirror

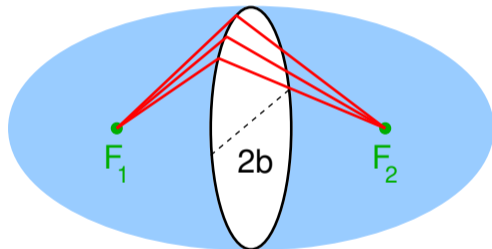


Ellipses are hard figures to make, so usually, they are approximated by circles. In the case of sagittal focusing, an ellipsoid of revolution with diameter  $2b$ , is used for focusing.

$$\rho_{\text{sagittal}} = b = 2f \sin \theta$$

The tangential focus is also usually approximated by a circular cross-section with radius

$$\rho_{\text{tangential}} = a = \frac{2f}{\sin \theta}$$



# Types of focusing mirrors



A simple mirror such as the one at MRCAT consists of a polished glass slab with two “legs”.



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The bimorph mirror is designed to obtain a smaller form error than a simple bender through the use of multiple actuators tuned experimentally.



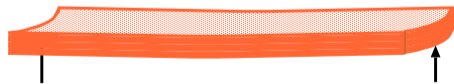


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A cost effective way to focus in both directions is a toroidal mirror which has a fixed bend in the transverse direction but which can be bent longitudinally to change the vertical focus.



# Dual focusing options





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- Kirkpatrick-Baez mirror pair — in combination with an **initial focusing element**, good for final small focal spot and variable energy

# Dual focusing options



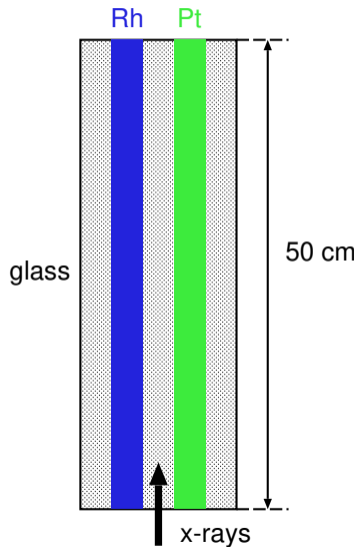
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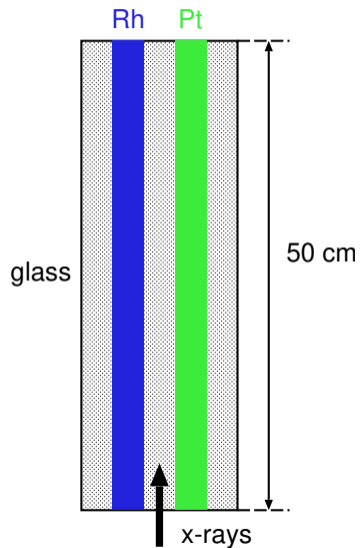


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- Zone plates — in combination with an **initial focusing element**, gives smallest focal spot, but hard to vary energy
- Refractive lenses — good final focus, focus moves with energy, significant attenuation and hard to change focal length

# The MRCAT mirror

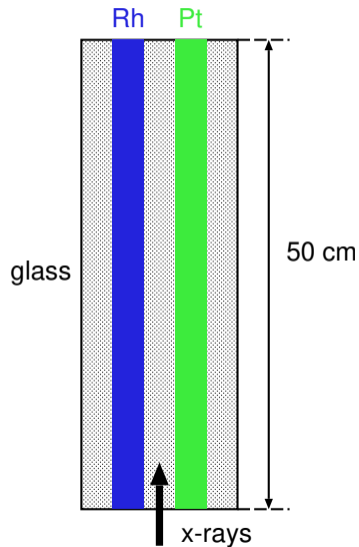


# The MRCAT mirror



Ultra low expansion glass polished to a few Å roughness

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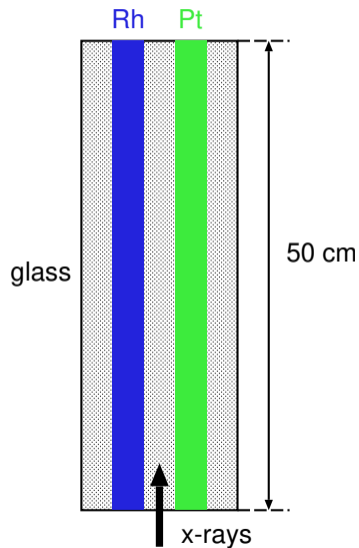


Ultra low expansion glass polished to a few Å roughness

One platinum stripe and one rhodium stripe deposited along the length of the mirror on top of a chromium buffer layer



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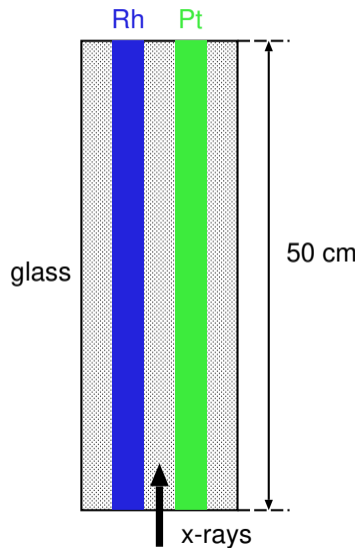


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A mounting system which permits angular positioning to less than 1/100 of a degree as well as horizontal and vertical motions

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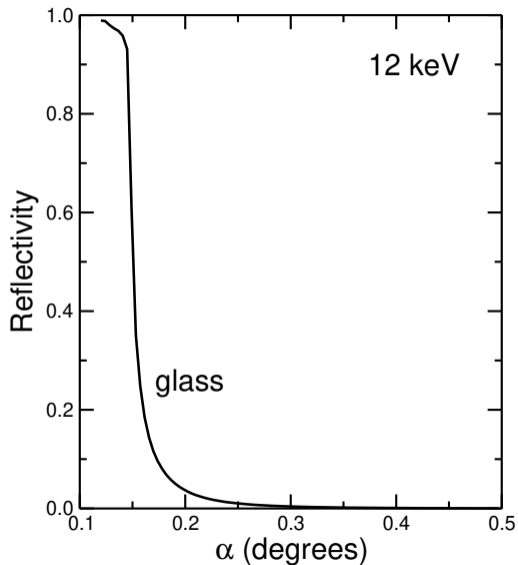
A mounting system which permits angular positioning to less than  $1/100$  of a degree as well as horizontal and vertical motions

A bending mechanism to permit vertical focusing of the beam to  $\sim 60 \mu\text{m}$

# Mirror performance



When illuminated with 12 keV x-rays on the glass “stripe”, the reflectivity is measured as:

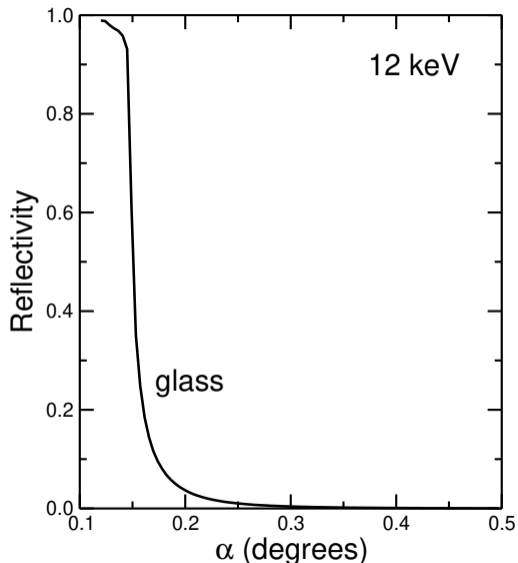


# Mirror performance



When illuminated with 12 keV x-rays on the glass “stripe”, the reflectivity is measured as:

With the Rh stripe, the thin slab reflection is evident and the critical angle is significantly higher.

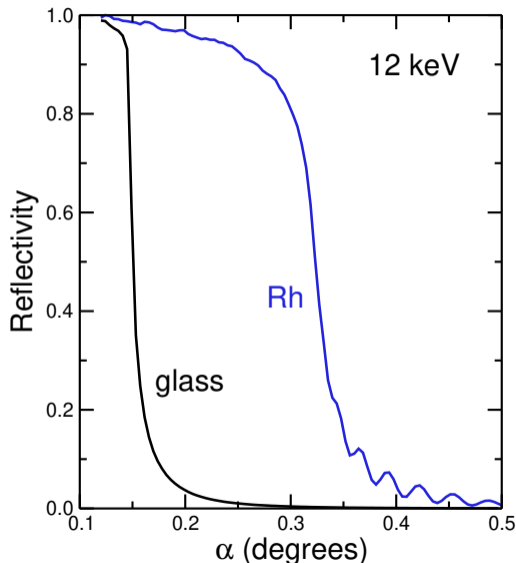


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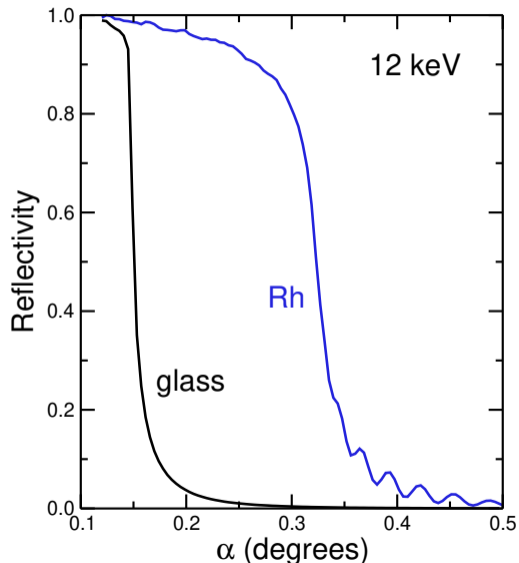
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The Pt stripe gives a higher critical angle still but a lower reflectivity and it looks like an infinite slab.



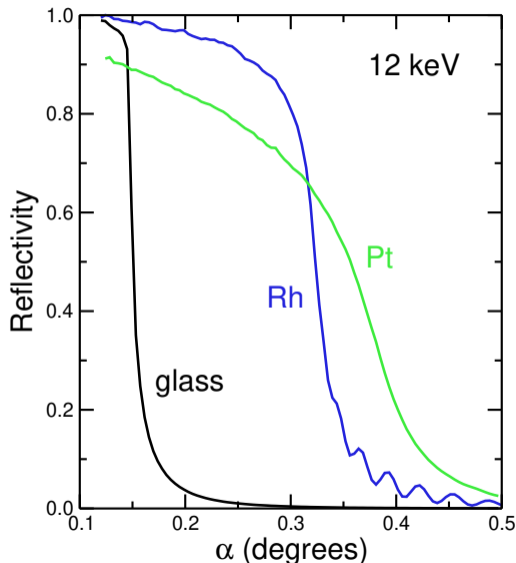
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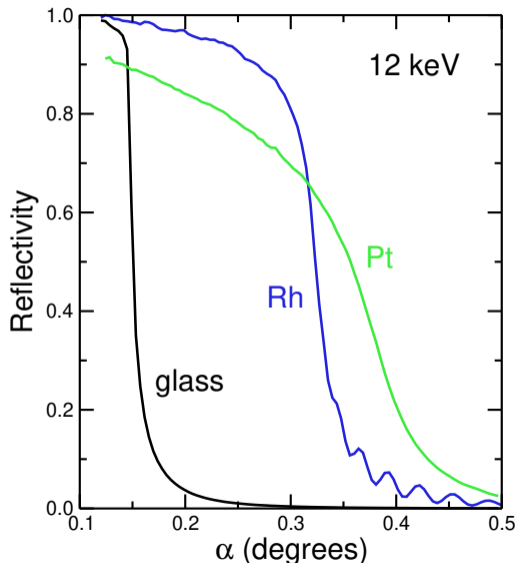


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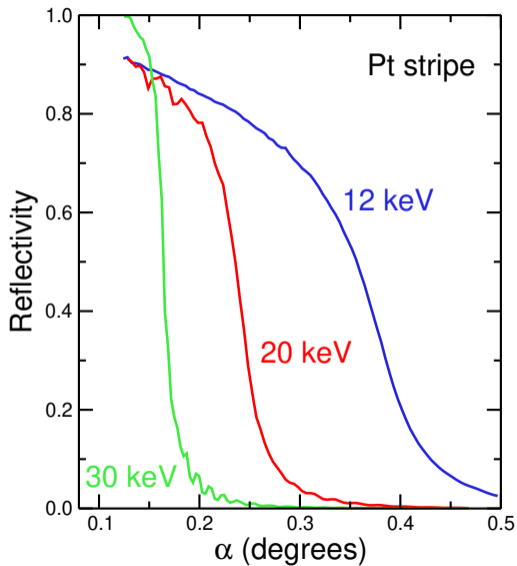
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Why?

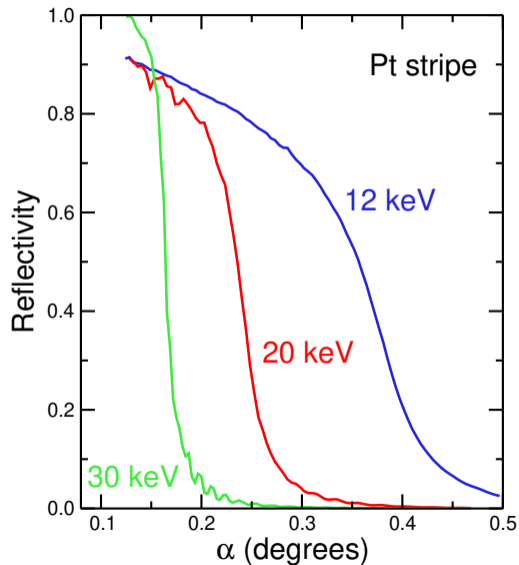




# Mirror performance (cont.)

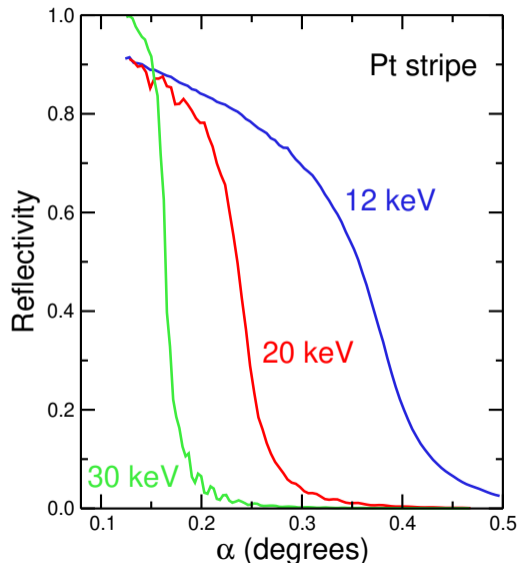


## Mirror performance (cont.)



As we move up in energy the critical angle for the Pt stripe drops.

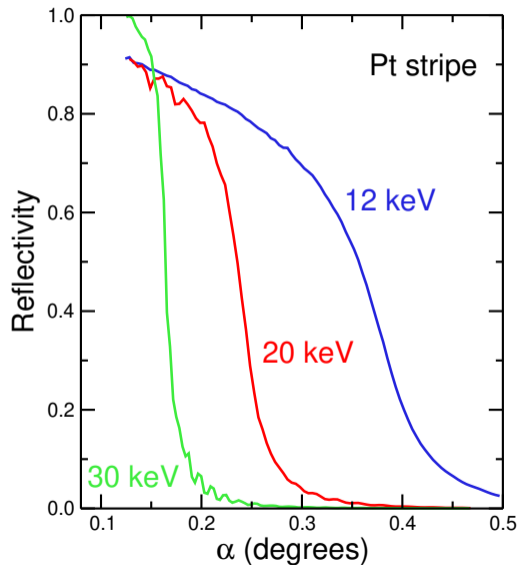
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The reflectivity at low angles improves as we are well away from the Pt absorption edges at 11,565 eV, 13,273 eV, and 13,880 eV.

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As energy rises, the Pt layer begins to show the reflectivity of a thin slab.

# Refractive optics



Just as with visible light, it is possible to make refractive optics for x-rays

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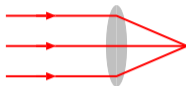


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visible light:

$$n \sim 1.2 - 1.5$$

$$f \sim 0.1\text{m}$$



# Refractive optics

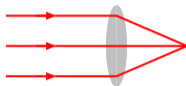


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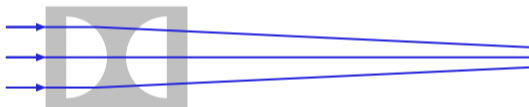
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x-rays:

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# Refractive optics

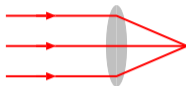


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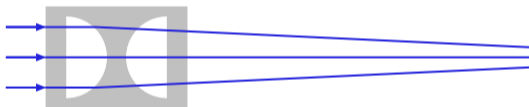
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x-ray lenses are complementary to those for visible light



# Refractive optics

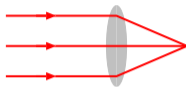


Just as with visible light, it is possible to make refractive optics for x-rays

visible light:

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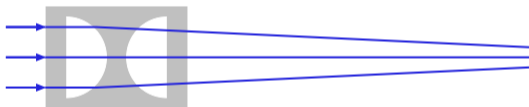
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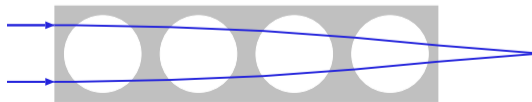
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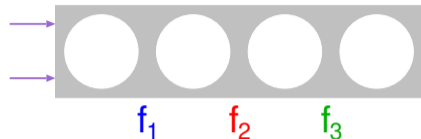
$$f \sim 100\text{m!}$$



x-ray lenses are complementary to those for visible light getting manageable focal distances requires making compound lenses

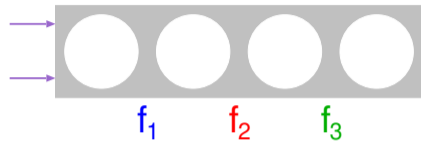


# Focal length of a compound lens



Start with a 3-element compound lens, calculate effective focal length

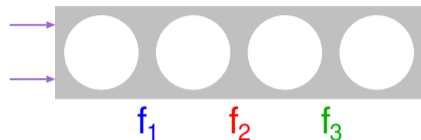
# Focal length of a compound lens



$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f}$$

Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length,  $f$

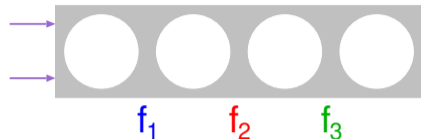
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$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f} \quad \longrightarrow \quad \frac{1}{i} = \frac{1}{f} - \frac{1}{o}$$

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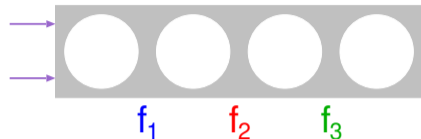


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$$\frac{1}{i_1} = \frac{1}{f_1} - \frac{1}{o_1}$$

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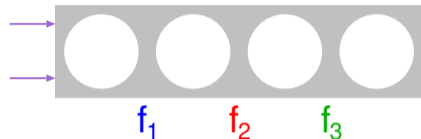
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$$f_1 = f, \quad o_1 = \infty$$

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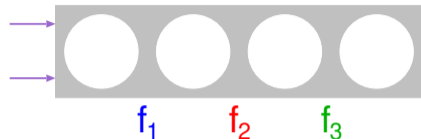
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$$\frac{1}{i_2} = \frac{1}{f_2} - \frac{1}{o_2}$$

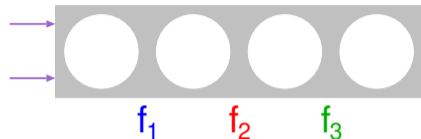
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for the second lens, the image  $i_1$  is a virtual object,  $o_2 = -i_1$



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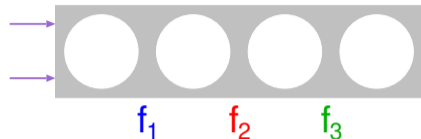
$$\frac{1}{i_2} = \frac{1}{f_2} - \frac{1}{o_2} \quad \longrightarrow \quad \frac{1}{i_2} = \frac{1}{f} + \frac{1}{f}$$

Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length,  $f$

$$f_1 = f, \quad o_1 = \infty$$

for the second lens, the image  $i_1$  is a virtual object,  $o_2 = -i_1$

# Focal length of a compound lens



$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f} \quad \longrightarrow \quad \frac{1}{i} = \frac{1}{f} - \frac{1}{o}$$

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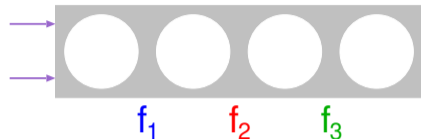
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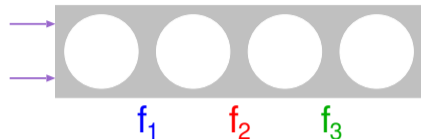
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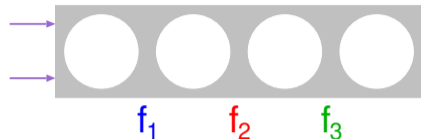
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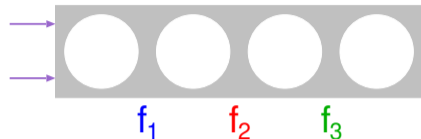
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so for  $N$  lenses  $f_{eff} = f/N$

## Rephasing distance



A spherical surface is not the ideal lens as it introduces aberrations. Derive the ideal shape for perfect focusing of x-rays.

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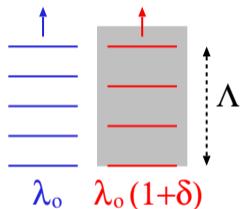
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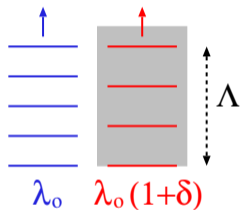
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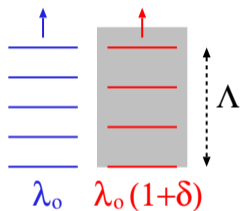
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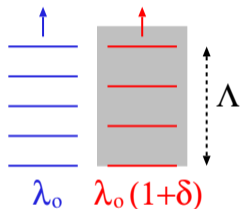
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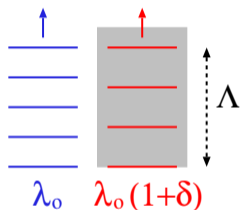
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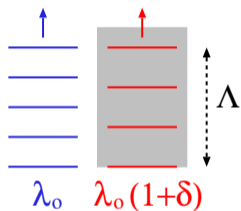
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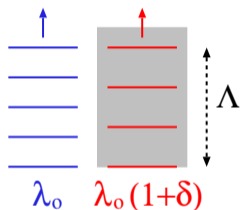
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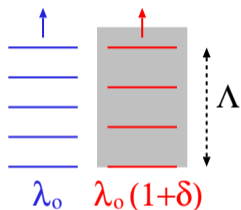
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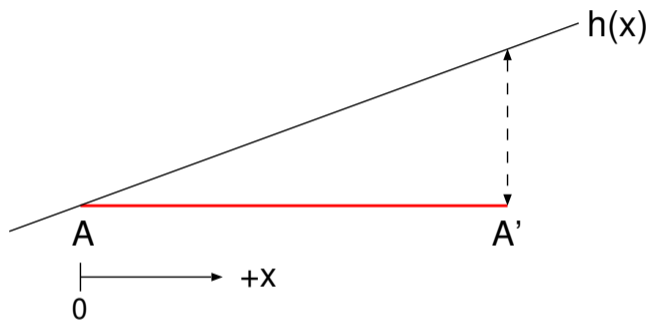
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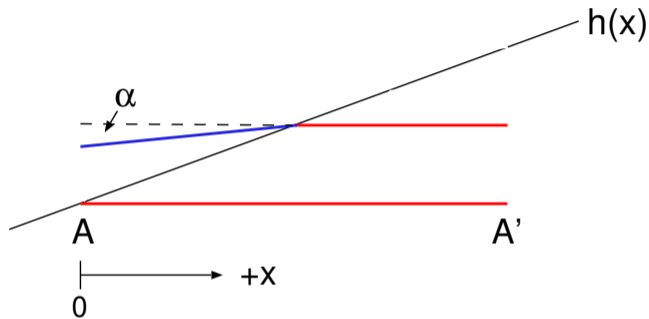
$$\Lambda = N\lambda_0 = \frac{\lambda_0}{\delta} = \frac{2\pi}{\lambda_0 r_0 \rho} \approx 10 \mu\text{m}$$



# Ideal interface profile - "thin" lens

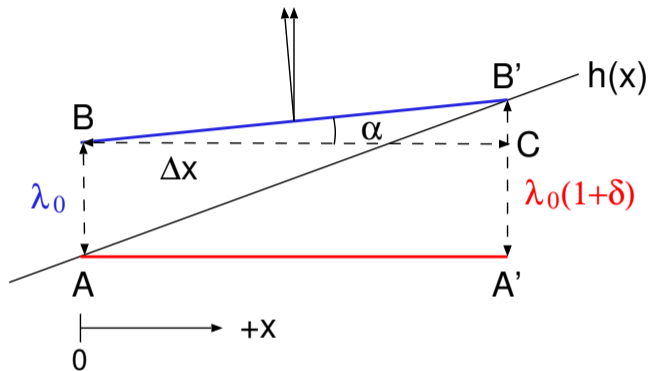


## Ideal interface profile - "thin" lens



The wave exits the material into vacuum through a surface of profile  $h(x)$ , and is twisted by an angle  $\alpha$ .

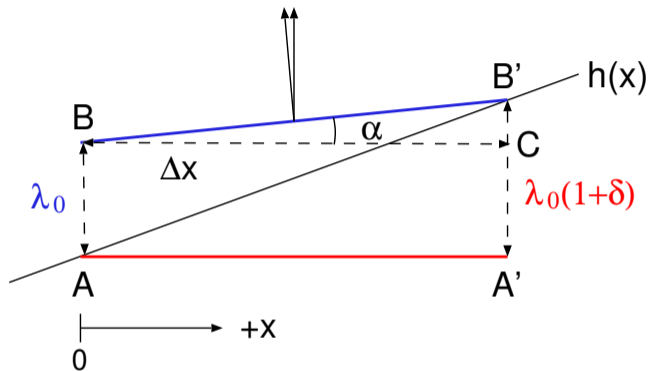
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The wave exits the material into vacuum through a surface of profile  $h(x)$ , and is twisted by an angle  $\alpha$ .

Follow the path of two points on the wavefront,  $A$  and  $A'$  as they propagate to  $B$  and  $B'$ .

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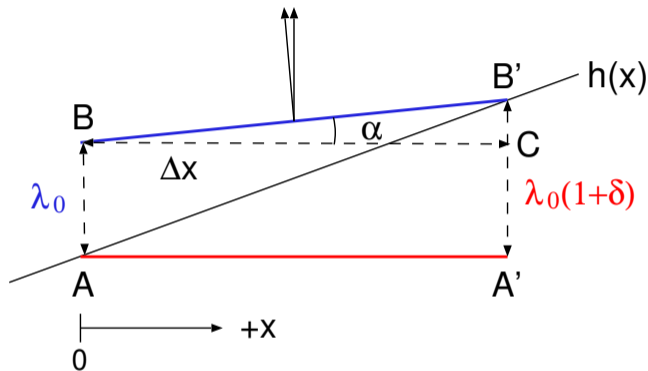


from the  $AA'B'$  triangle

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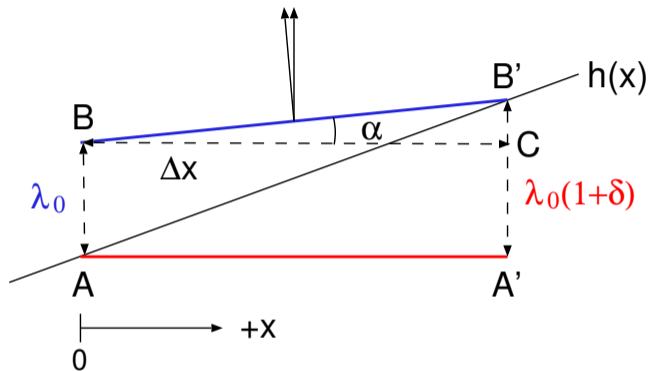
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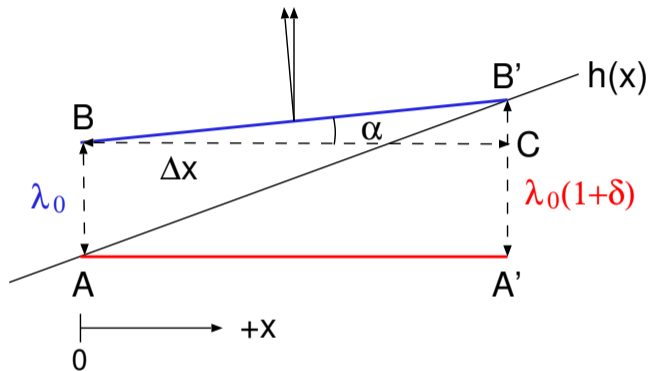
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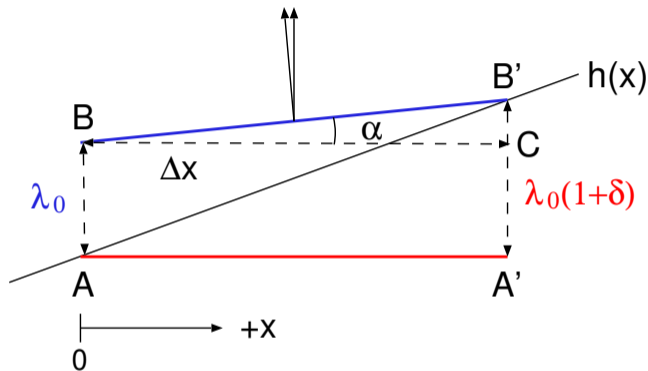
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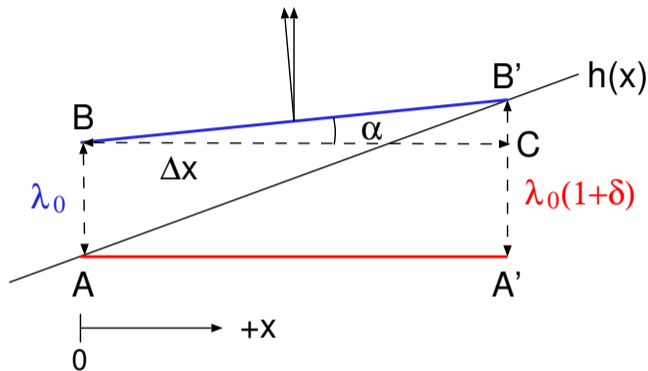
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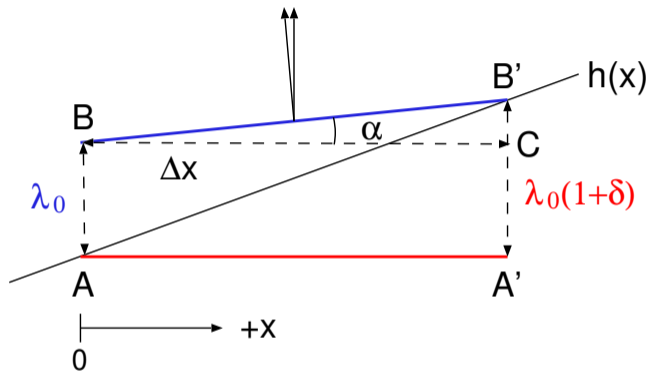
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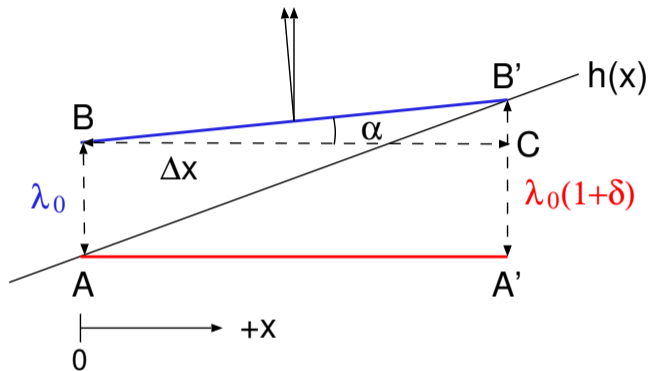
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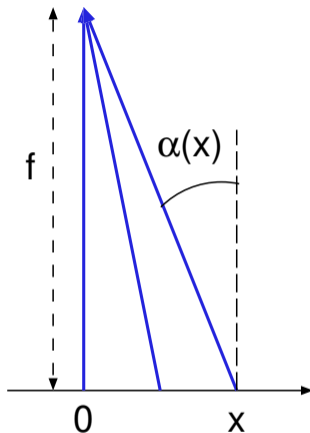
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## Ideal interface profile - "thin" lens

If the desired focal length of this lens is  $f$ , the wave must be redirected at an angle which depends on the distance from the optical axis

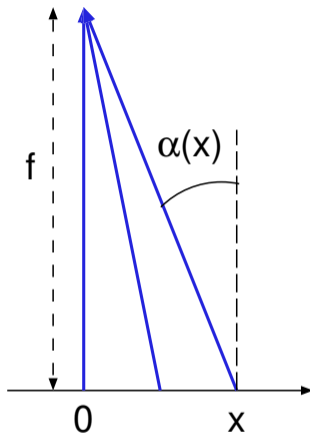




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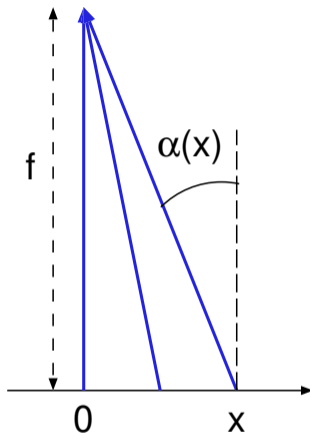
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combining, we have

$$\frac{\lambda_0 h'(x)}{\Lambda} = \frac{x}{f}$$





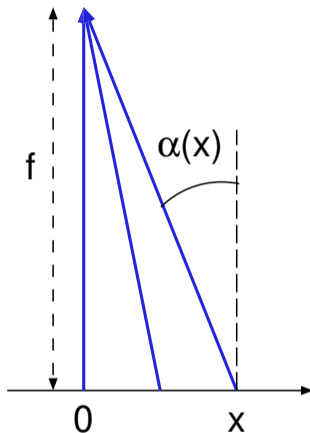
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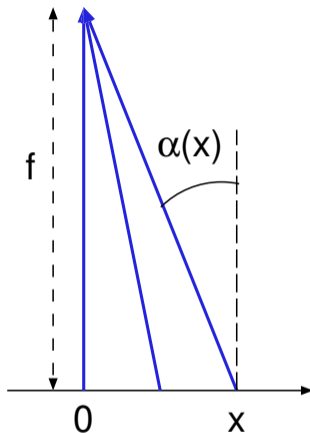
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this can be directly integrated







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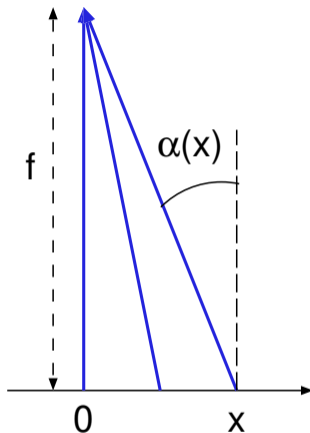
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$$\frac{h(x)}{\Lambda} = \frac{x^2}{2f \lambda_0}$$





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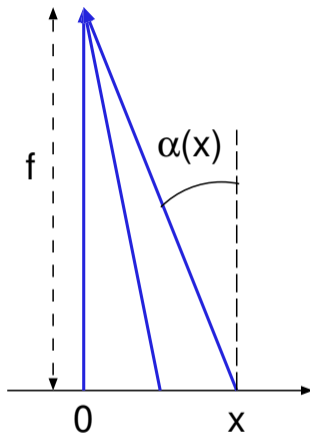
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$$\frac{h(x)}{\Lambda} = \frac{x^2}{2f \lambda_0} = \left[ \frac{x}{\sqrt{2f \lambda_0}} \right]^2$$





## Ideal interface profile - “thin” lens

If the desired focal length of this lens is  $f$ , the wave must be redirected at an angle which depends on the distance from the optical axis

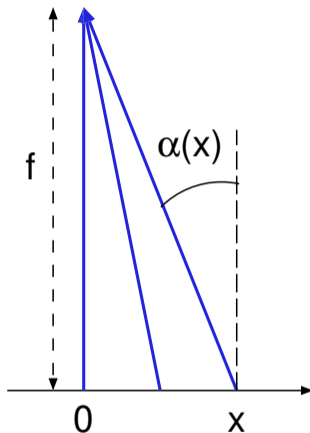
$$\alpha(x) = \frac{x}{f}$$

combining, we have

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a parabola is the ideal surface shape for focusing by refraction for a “thin” lens with limited aperture

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From the previous expression for the ideal parabolic surface, the focal length can be written in terms of the surface profile.

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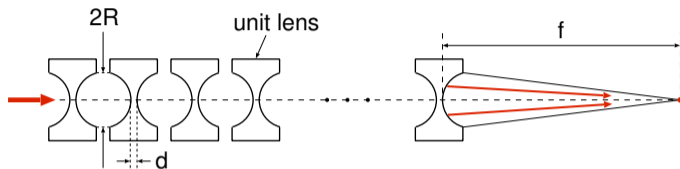
and thus the focal length becomes

for  $2N$  circular lenses we have

$$\begin{aligned} h(x) &= R - \sqrt{R^2 - x^2} = R - R\sqrt{1 - \frac{x^2}{R^2}} \\ &\approx R - R\left(1 - \frac{1}{2} \frac{x^2}{R^2}\right) \approx \frac{x^2}{2R} \\ f &\approx \frac{R}{\delta} \\ f_{2N} &\approx \frac{R}{2N\delta} \end{aligned}$$

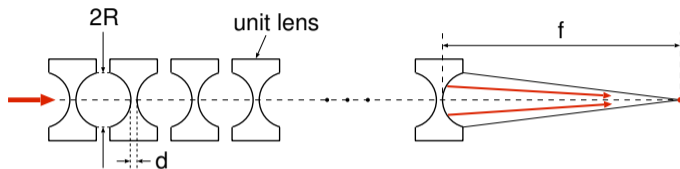


# Focussing by a beryllium lens



H.R. Beguiristain et al., "X-ray focusing with compound lenses made from beryllium," *Optics Lett.*, **27**, 778 (2007).

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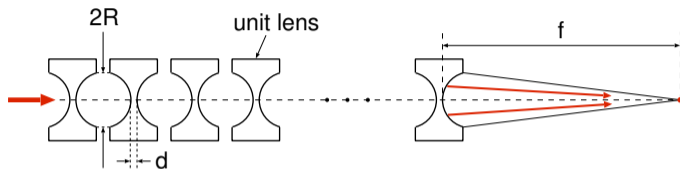


For 50 holes of radius  $R = 1\text{mm}$  in beryllium (Be) at  $E = 10\text{keV}$ , we can calculate the focal length, knowing  $\delta = 3.41 \times 10^{-6}$

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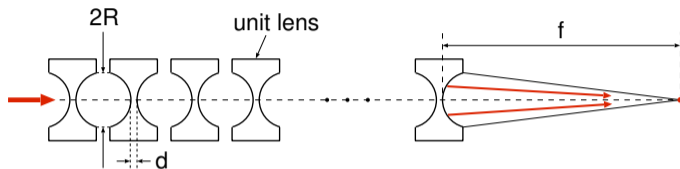


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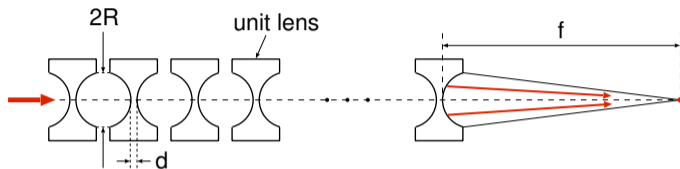


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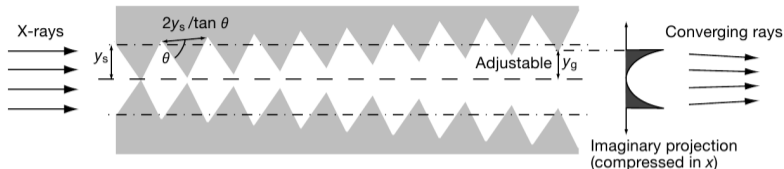
depending on the wall thickness of the lenslets, the transmission can be up to 74%

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# Alligator-type lenses



Perhaps one of the most original x-ray lenses has been made by using old vinyl records in an “alligator” configuration.

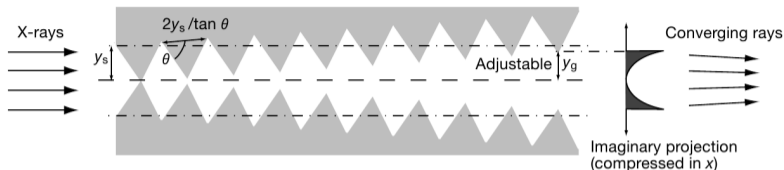


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This design has also been used to make lenses out of lithium metal.

E.M. Dufresne et al., “Lithium metal for x-ray refractive optics”, *Appl. Phys. Lett.* **79**, 4085 (2001).

# Extruded Al lens



The compound refractive lenses (CRL) are useful for fixed focus but are difficult to use if a variable focal distance and a long focal length is required.

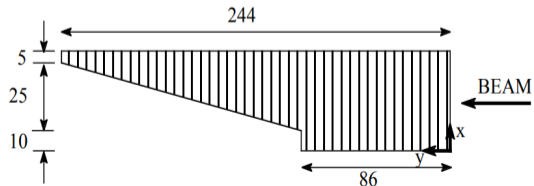
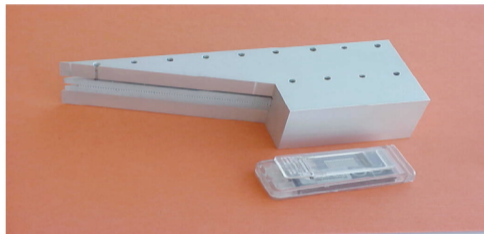
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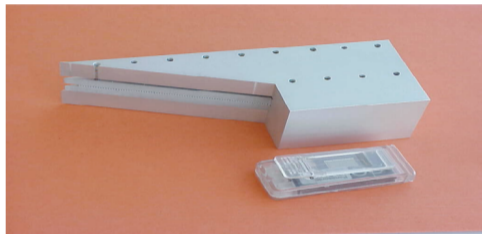


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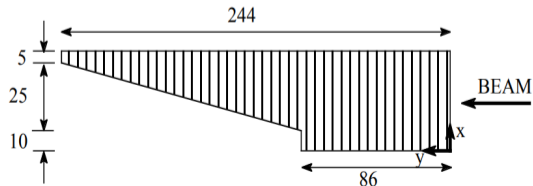
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Extruded aluminum lens with parabolic figure

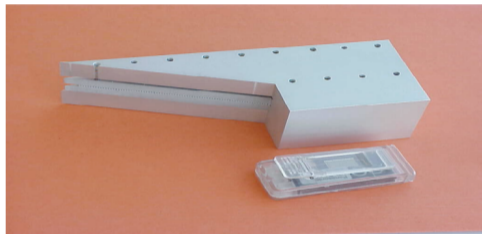


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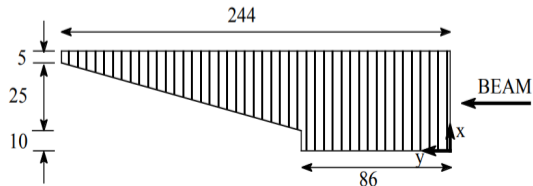


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Cut diagonally to expose variable number of “lenses” to a horizontal beam

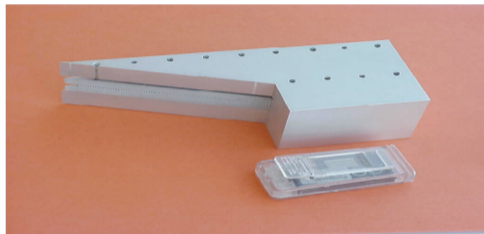


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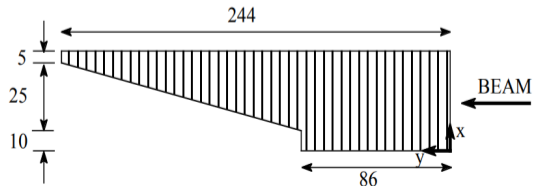
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Extruded aluminum lens with parabolic figure

Cut diagonally to expose variable number of “lenses” to a horizontal beam

Horizontal translation allows change in focal length but it is quantized, not continuous



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## Variable focal length CRL



A continuously variable focal length is very important for two specific reasons: tracking sample position, and keeping the focal length constant as energy is changed.

## Variable focal length CRL



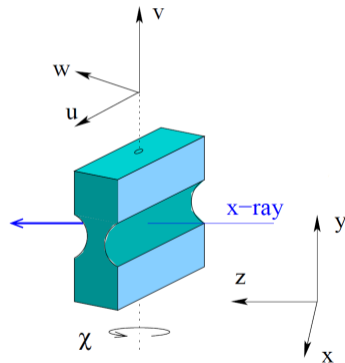
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Start with a 2 hole CRL.



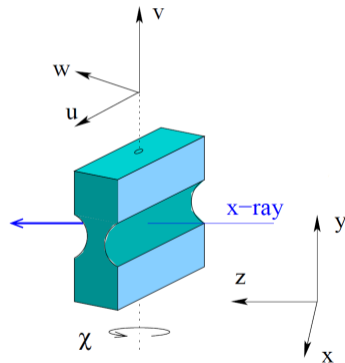
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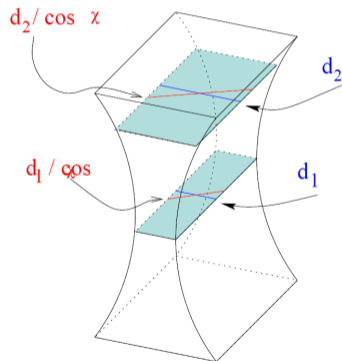




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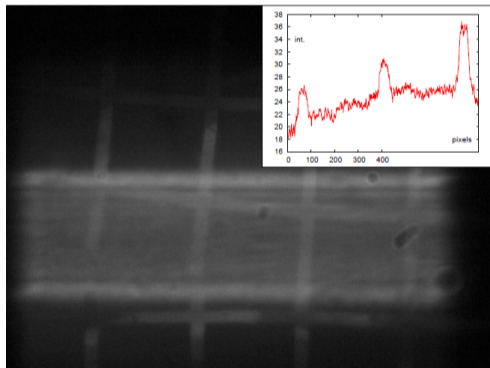


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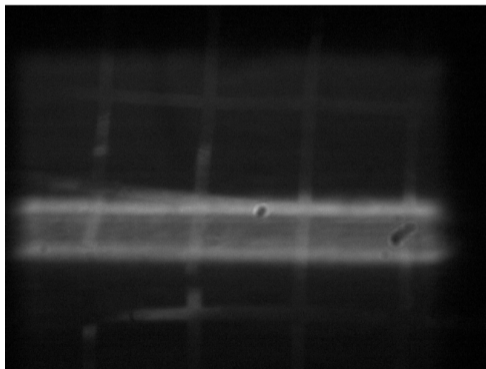


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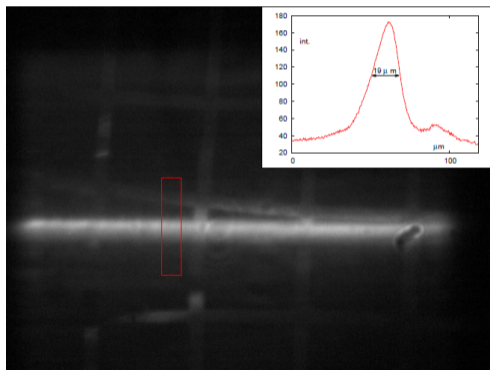
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Optimal focus is  $20\mu\text{m}$  at  $\chi = 40^\circ$



# Polycapillary optics



A polycapillary is a focusing optic made up of an array of thousands of thin-walled hollow tubes which are  $> 65\%$  empty space

F.A. Hofmann et al., "Focusing of synchrotron radiation with polycapillary optics,"  
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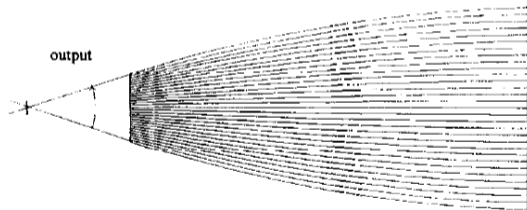
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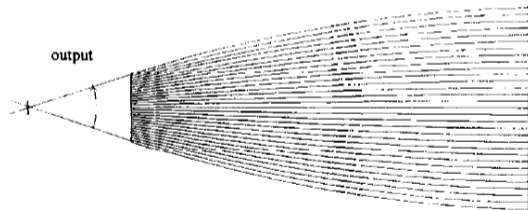
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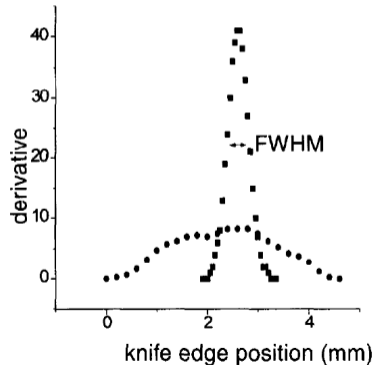


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# Improving polycapillary optic performance



One drawback of a glass capillary is that the transmission at high energies is reduced because of critical angle restrictions

M.A. Popecki et al., "Development of polycapillary x-ray optics for synchrotron spectroscopy," *Proc. SPIE* **9588**, 95880D (2015).

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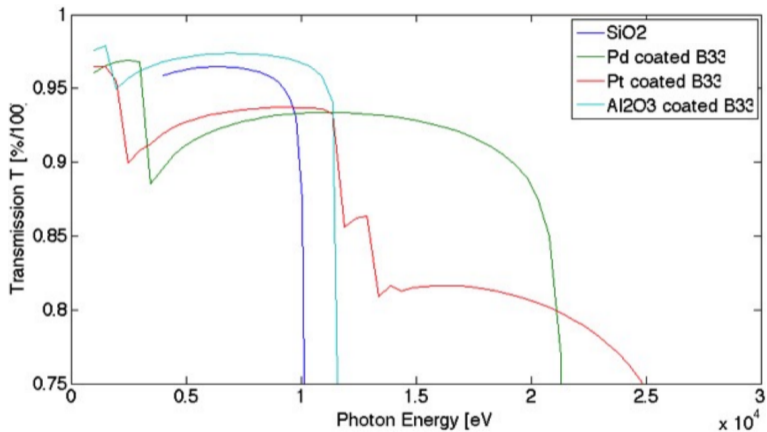
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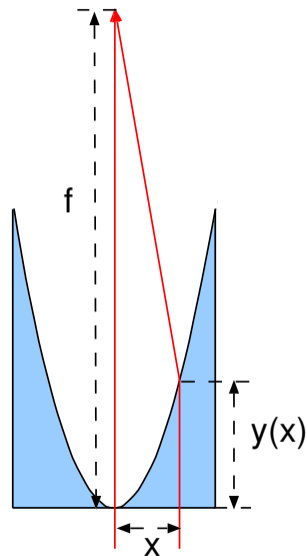
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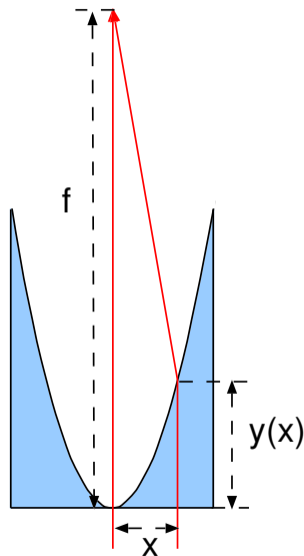
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The two rays shown must be in phase when they reach the focal point and so we can write





# Elliptical lens surface



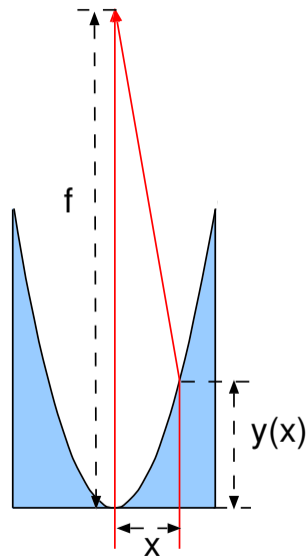
In calculating the optimal surface profile for a refractive lens, an important approximation was made which resulted in a parabolic surface

The assumption was made that only a small portion of the lens area along the axis was illuminated

What happens if we lift this restriction?

The two rays shown must be in phase when they reach the focal point and so we can write

$$f = y(1 - \delta) + \sqrt{(f - y)^2 + x^2}$$



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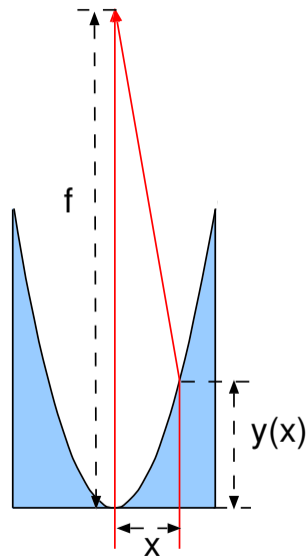
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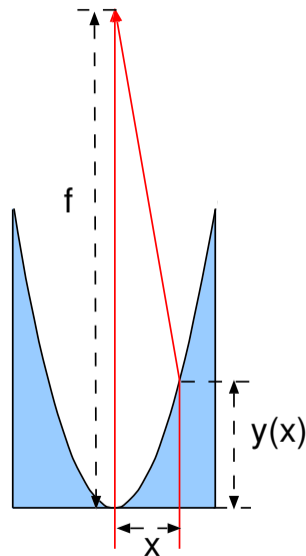
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$$2f\delta y - (2\delta - \delta^2)y^2 = x^2$$



# Elliptical lens surface



Ideal surface

Ellipse

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Ideal surface

$$0 = x^2 + (2\delta - \delta^2)y^2 - 2f\delta y$$

Ellipse

$$1 = \frac{x^2}{a^2} + \frac{(y - b)^2}{b^2}$$

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The ideal surface for a thick lens is an ellipse