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Powder diffraction



- Powder diffraction
- Pair distribution function



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- Bragg & Laue geometries

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Reading Assignment: Chapter 6.1-6.2



- Powder diffraction
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- Bragg & Laue geometries

Reading Assignment: Chapter 6.1-6.2

Homework Assignment #04: Chapter 4: 2,4,6,7.10 due Tuesday, October 19, 2021

- Powder diffraction
- Pair distribution function
- Bragg & Laue geometries

Reading Assignment: Chapter 6.1-6.2

Homework Assignment #04: Chapter 4: 2,4,6,7.10 due Tuesday, October 19, 2021 Homework Assignment #05: Chapter 5: 1,3,7,9,10 due Tuesday, November 02, 2021



$$\left\langle e^{iQ(u_{Qm}-u_{Qn})} \right\rangle = e^{-Q^2 \langle u_{Qm}^2 \rangle/2} e^{-Q^2 \langle u_{Qn}^2 \rangle/2} e^{Q^2 \langle u_{Qm}u_{Qn} \rangle}$$



$$ig\langle e^{iQ(u_{Qm}-u_{Qn})}ig
angle = e^{-Q^2\langle u_{Qm}^2
angle/2}e^{-Q^2\langle u_{Qn}^2
angle/2}e^{Q^2\langle u_{Qm}u_{Qn}
angle}
onumber \ = e^{-Q^2\langle u_Q^2
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angle}$$



$$ig\langle e^{iQ(u_{Q_m}-u_{Q_n})}ig
angle = e^{-Q^2\langle u_{Q_m}^2
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angle}
onumber \ = e^{-Q^2\langle u_Q^2
angle}e^{Q^2\langle u_{Q_m}u_{Q_n}
angle} = e^{-2M}e^{Q^2\langle u_{Q_m}u_{Q_n}
angle}$$



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$$= e^{-Q^2 \langle u_{Q}^2 \rangle} e^{Q^2 \langle u_{Qm}u_{Qn} \rangle} = e^{-2M} e^{Q^2 \langle u_{Qm}u_{Qn} \rangle} = e^{-2M} \left[1 + e^{Q^2 \langle u_{Qm}u_{Qn} \rangle} - 1 \right]$$



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Substituting into the expression for intensity



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Substituting into the expression for intensity

$$I = \sum_{m} \sum_{n} f(\vec{Q}) e^{-M} e^{i\vec{Q}\cdot\vec{R}_{m}} f^{*}(\vec{Q}) e^{-M} e^{-i\vec{Q}\cdot\vec{R}_{n}} + \sum_{m} \sum_{n} f(\vec{Q}) e^{-M} e^{i\vec{Q}\cdot\vec{R}_{m}} f^{*}(\vec{Q}) e^{-M} e^{-i\vec{Q}\cdot\vec{R}_{n}} \left[e^{Q^{2} \langle u_{Qm} u_{Qn} \rangle} - 1 \right]$$



$$\left\langle e^{iQ(u_{Qm}-u_{Qn})} \right\rangle = e^{-Q^2 \langle u_{Qm}^2 \rangle / 2} e^{-Q^2 \langle u_{Qn}^2 \rangle / 2} e^{Q^2 \langle u_{Qm}u_{Qn} \rangle}$$
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$$+ \sum_{m} \sum_{n} f(\vec{Q}) e^{-M} e^{i\vec{Q}\cdot\vec{R}_{m}} f^{*}(\vec{Q}) e^{-M} e^{-i\vec{Q}\cdot\vec{R}_{n}} \left[e^{Q^{2}\langle u_{Qm}u_{Qn}\rangle} - 1 \right]$$

The first term is just the elastic scattering from the lattice with the addition of the term $e^{-M} = e^{-Q^2 \langle u_Q^2 \rangle/2}$, called the Debye-Waller factor.

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The first term is just the elastic scattering from the lattice with the addition of the term $e^{-M} = e^{-Q^2 \langle u_Q^2 \rangle/2}$, called the Debye-Waller factor.

The second term is the Thermal Diffuse Scattering and actually increases with mean squared displacement.

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$$I^{TDS} = \sum_{m} \sum_{n} f(\vec{Q}) e^{-M} e^{i\vec{Q}\cdot\vec{R}_{m}} f^{*}(\vec{Q}) e^{-M} e^{-i\vec{Q}\cdot\vec{R}_{n}} \left[e^{Q^{2} \langle u_{Qm}u_{Qn} \rangle} - 1 \right]$$



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The TDS has a width determined by the correlated displacement of atoms which is much broader than a Bragg peak.



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These correlated motions are just phonons.



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"Determination of phonon dispersions from x-ray transmission scattering: The example of silicon," M. Holt, et al. *Phys. Rev. Lett.* **83**, 3317 (1999).



incident beam along (100)



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incident beam along (111)



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dotted line from this measurement

V



$$\mathcal{F}^{u.c.} = \sum_j f_j(\vec{Q}) e^{-M_j} e^{i \vec{Q} \cdot \vec{r}_j}$$



$$egin{aligned} \mathcal{F}^{u.c.} &= \sum_{j} f_{j}(ec{Q}) e^{-M_{j}} e^{i ec{Q} \cdot ec{r}_{j}} \ M_{j} &= rac{1}{2} Q^{2} \langle u_{Qj}^{2}
angle \end{aligned}$$



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angle = rac{1}{2} \left(rac{4\pi}{\lambda}
ight)^{2} \sin^{2} heta \langle u_{Qj}^{2}
angle \end{aligned}$$



$$B_T^j = 8\pi^2 \langle u_{Qj}^2 \rangle$$

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For crystals with several different types of atoms, we generalize the unit cell scattering factor.

$$B_T^j = 8\pi^2 \langle u_{Qj}^2 \rangle$$

for isotropic atomic vibrations

$$\langle u^2 \rangle = \langle u_x^2 + u_y^2 + u_z^2 \rangle$$

= $3 \langle u_x^2 \rangle = 3 \langle u_Q^2 \rangle$

$$egin{aligned} & \nabla^{u.c.} = \sum_{j} f_{j}(ec{Q}) e^{-M_{j}} e^{i ec{Q} \cdot ec{r}_{j}} \ & M_{j} = rac{1}{2} Q^{2} \langle u_{Qj}^{2}
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1

$$\begin{split} \langle u^2 \rangle &= \langle u_x^2 + u_y^2 + u_z^2 \rangle \\ &= 3 \langle u_x^2 \rangle = 3 \langle u_Q^2 \rangle \end{split}$$

$$F^{u.c.} = \sum_{j} f_{j}(\vec{Q}) e^{-M_{j}} e^{i\vec{Q}\cdot\vec{r}_{j}}$$
$$M_{j} = \frac{1}{2} Q^{2} \langle u_{Qj}^{2} \rangle = \frac{1}{2} \left(\frac{4\pi}{\lambda}\right)^{2} \sin^{2}\theta \langle u_{Qj}^{2} \rangle$$
$$M_{j} = B_{T}^{j} \left(\frac{\sin\theta}{\lambda}\right)^{2}$$
$$B_{T}^{iso} = \frac{8\pi^{2}}{3} \langle u^{2} \rangle$$



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In general, Debye-Waller factors can be anisotropic



The Debye model can be used to compute B_T by integrating a linear phonon dispersion relation up to a cutoff frequency, ω_D , called the Debye frequency.

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$$B_T = rac{6h^2}{m_A k_B \Theta} \left[rac{\phi(\Theta/T)}{\Theta/T} + rac{1}{4}
ight]$$





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$$B_{T} = \frac{6h^{2}}{m_{A}k_{B}\Theta} \left[\frac{\phi(\Theta/T)}{\Theta/T} + \frac{1}{4}\right]$$
$$\phi(x) = \frac{1}{x} \int_{0}^{\Theta/T} \frac{\xi}{e^{\xi} - 1} d\xi$$





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$$B_{\mathcal{T}}[\text{\AA}^2] = \frac{11492\text{T}[\text{K}]}{\text{A}\Theta^2[\text{K}^2]}\phi(\Theta/\text{T}) + \frac{2873}{\text{A}\Theta[\text{K}]}$$



Debye Temperatures



	Α	Θ	B _{4.2}	B ₇₇	B ₂₉₃
		(K)		(Ų)	
C*	12	2230	0.11	0.11	0.12
AI	27	428	0.25	0.30	0.72
Cu	63.5	343	0.13	0.17	0.47
*diamond					

 $B_T = \frac{11492T}{A\Theta^2}\phi(\Theta/T) + \frac{2873}{A\Theta}$

diamond
Debye Temperatures



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$$B_{\mathcal{T}} = rac{11492\,T}{\mathcal{A}\Theta^2}\phi(\Theta/\,T) + rac{2873}{\mathcal{A}\Theta}$$

diamond is very stiff and $\boldsymbol{\Theta}$ does not vary much with temperature

Debye Temperatures



	A	Θ	B _{4.2}	B ₇₇	B_{293}	
		(K)		(Ų)		
C*	12	2230	0.11	0.11	0.12	
AI	27	428	0.25	0.30	0.72	
Cu	63.5	343	0.13	0.17	0.47	
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 $B_{T} = \frac{11492T}{A\Theta^{2}}\phi(\Theta/T) + \frac{2873}{A\Theta}$

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copper has a much lower Debye temperature and a wider variation of thermal factor with temperature

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Beamline 11BM at the APS





"A dedicated powder diffraction beamline at the Advanced Photon Source: Commissioning and early operational results," J. Wang et al. Rev. Sci. Instrum. 79, 085105 (2008).

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Beamline 11BM at the APS





2D detectors have limited angular resolution, for high resolution routine powder diffraction, beamlines such as 11BM are ideal

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Beamline 11BM at the APS





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The initial collimating mirror makes the beam more parallel and then it is focused horizontally and vertically to the sample

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[&]quot;A dedicated powder diffraction beamline at the Advanced Photon Source: Commissioning and early operational results," J. Wang et al. Rev. Sci. Instrum. 79, 085105 (2008).



"A twelve-analyzer detector system for high resolution powder diffraction," P.L. Lee et al. J. Synch. Rad. 15, 427-432

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High throughput is obtained using a robot arm to change samples

"A twelve-analyzer detector system for high resolution powder diffraction," P.L. Lee et al. J. Synch. Rad. 15, 427-432

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V

High throughput is obtained using a robot arm to change samples

The sample is mounted on a rotating spindle at the center of the goniometer

"A twelve-analyzer detector system for high resolution powder diffraction," P.L. Lee et al. J. Synch. Rad. 15, 427-432

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High throughput is obtained using a robot arm to change samples

The sample is mounted on a rotating spindle at the center of the goniometer

High resolution is achieved with a 12 crystal analyzer system which is rotated on the main circle of the goniometer

"A twelve-analyzer detector system for high resolution powder diffraction," P.L. Lee et al. J. Synch. Rad. 15, 427-432







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Each of the 12 analyzer crystals is tuned to the desired scattering energy and as the entire assembly is scanned, all twelve banks are collecting data and then are merged

"A twelve-analyzer detector system for high resolution powder diffraction," P.L. Lee et al. J. Synch. Rad. 15, 427-432

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The analyzer and robot arm



"A twelve-analyzer detector system for high resolution powder diffraction," P.L. Lee et al. J. Synch. Rad. 15, 427-432

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The analyzer and robot arm



Samples are in Kapton capillaries and magnetic bases for remote mounting



"A twelve-analyzer detector system for high resolution powder diffraction," P.L. Lee et al. J. Synch. Rad. 15, 427-432

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Data from high resolution LaB₆ standard



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Data from high resolution LaB₆ standard



High resolution data with high count rates can be obtained out to very high angles with a wavelength of $\lambda \approx 0.5$ Å.

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Refinement of SiO_2 and AI_2O_3





"A dedicated powder diffraction beamline at the Advanced Photon Source: Commissioning and early operational results," J. Wang et al. Rev. Sci. Instrum. 79,

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V

CaO is a possible material to be used for carbon sequestration

A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, Chemical Eng. Sci. 127, 13-24 (2015)

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CaO is a possible material to be used for carbon sequestration

CaO will absorb CO₂ at temperatures as low as 450° C forming CaCO₃ and can be regenerated by calcination at temperatures above 700° C

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It is important to understand the fundamental reaction kinetics of thse processes in order to be able to design carbon sequestration procedures.

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Measurements heretofore have been performed in TGA systems which have fundamental mass flow limitations. These experiments were performed at Sector 17-BM of the APS. Samples were loaded in quartz capillaries and a 2D area detector was used to take snaps at up to 0.25s/frame.

A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, Chemical Eng. Sci. 127, 13-24 (2015)

CaO-CaO₂ reaction kinetics



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Rietveld refinement was used to measure the lattice parameters, crystallite sizes and phase fractions during carbonation and calcination cycles

A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, Chemical Eng. Sci. 127, 13-24 (2015)

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Typical diffraction pattern



A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, Chemical Eng. Sci. 127, 13-24 (2015)

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Final conversion fraction





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Final conversion fraction





Final conversion fraction depends on temperature but also some other parameter (what?)

A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, *Chemical Eng. Sci.* **127**, 13-24 (2015)

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Final conversion fraction





Final conversion fraction depends on temperature but also some other parameter (what?)

Remember that these powders have only been seived to a particular grain size, what about the internal structure?

A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, *Chemical Eng. Sci.* **127**, 13-24 (2015)

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A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, *Chemical Eng. Sci.* **127**, 13-24 (2015)





Because of the high speed of the 2D detector, it is possible to look at the conversion reaction at unprecedented time scales

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Because of the high speed of the 2D detector, it is possible to look at the conversion reaction at unprecedented time scales

Reaction kinetics much faster, $1/\tau=0.28~{\rm s}^{-1},$ than previously observed with TGA measurements

A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, *Chemical Eng. Sci.* **127**, 13-24 (2015)

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The rates of conversion are determined by fitting the initial (up to 50%) slope of the phase fraction as a function of time with a straight line

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CaO-CaO₂ reaction kinetics





Initial crystallite size is one of the determining factors in initial rate of conversion and fraction converted.

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CaO crystallite size can be related to porosity which is key to the conversion process.

A. Biasin, C.U. Segre, G. Salviulo, F. Zorzi, and M. Strumendo, Chemical Eng. Sci. 127, 13-24 (2015)

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Pair distribution function



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So what does the pair distribution function look like in practice?

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PDF processing: F(Q) and G(r)



"Local environment of terbium(III) ions in layered nanocrystalline zirconium(IV) phosphate – phosphate ion exchange materials," M.W. Terban, et al. *Inorg. Chem.* **56**, 8837-8846 (2017).

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When Fourier transformed, the significant differences in crystalline and nanoparticulate samples are obvious

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The goal of this study was to compare the PDF structures of CdSe nanoparticles of various sizes with the results obtained from traditional analysis of optical data and electron microscopy

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Optical absorbance and fluorescence indicates particle sizes ranging from 3.5 nm to 2.0 nm

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PDF data collection



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Data were collected on bulk CdSe (left)

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Data were collected on bulk CdSe (left) and the CdSe nanoparticles (right) then azimuthally integrated to get the powder pattern





The data for bulk and nanoparticle samples was processed to obtain F(Q) and G(r) in preparation for structural modeling



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The particle size progression shows in the range over which the G(r)has distinct peak structure






The first fit to the data uses the wurtzite structure which has ABAB stacking of hexagonal planes

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It is likely that a better fit can be obtained using a mixture of the two stacking arrangements

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Final structural models





A fit using both wurtzite and zinc blende fits much better for all particles

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The final values obtained in the fitting give particle sizes consistent with TEM and optical measurements. The fits also show that the bulk sample has only about 33% stacking faults while the nanoparticles have 50%

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