

Today's outline - September 23, 2021



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- Refractive optics

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- Refractive optics
- Ideal refractive surface

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- Fresnel lenses and zone plates

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- Research papers on refraction

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Reading Assignment: Chapter 4.1–4.2

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- Refractive optics
- Ideal refractive surface
- Fresnel lenses and zone plates
- Research papers on refraction

Reading Assignment: Chapter 4.1–4.2

Homework Assignment #03:

Chapter 3: 1,3,4,6,8

due Tuesday, October 05, 2021

Today's outline - September 23, 2021



- Refractive optics
- Ideal refractive surface
- Fresnel lenses and zone plates
- Research papers on refraction

Reading Assignment: Chapter 4.1–4.2

Homework Assignment #03:

Chapter 3: 1,3,4,6,8

due Tuesday, October 05, 2021

Homework Assignment #04:

Chapter 4: 2,4,6,7,10

due Tuesday, October 19, 2021

Refractive optics



Just as with visible light, it is possible to make refractive optics for x-rays

Refractive optics

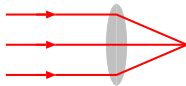


Just as with visible light, it is possible to make refractive optics for x-rays

visible light:

$$n \sim 1.2 - 1.5$$

$$f \sim 0.1\text{m}$$



Refractive optics

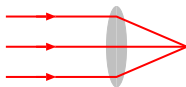


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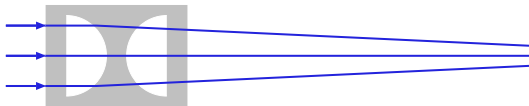
$$f \sim 0.1\text{m}$$



x-rays:

$$n \approx 1 - \delta, \delta \sim 10^{-5}$$

$$f \sim 100\text{m!}$$



Refractive optics

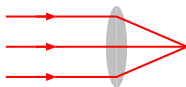


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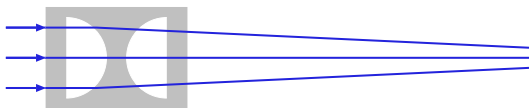
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x-ray lenses are complementary to those for visible light

Refractive optics

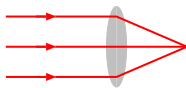


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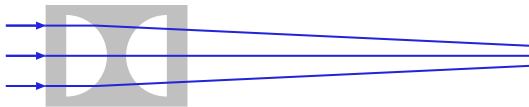
$$f \sim 0.1\text{m}$$



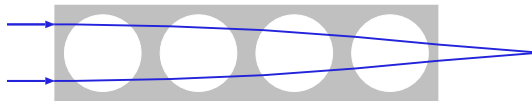
x-rays:

$$n \approx 1 - \delta, \delta \sim 10^{-5}$$

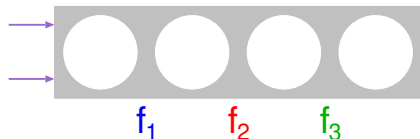
$$f \sim 100\text{m!}$$



x-ray lenses are complementary to those for visible light getting manageable focal distances requires making compound lenses

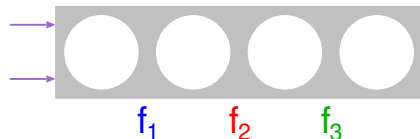


Focal length of a compound lens



Start with a 3-element compound lens, calculate effective focal length

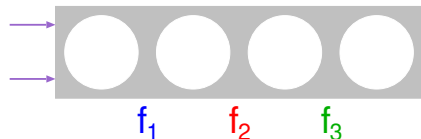
Focal length of a compound lens



$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f}$$

Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length, f

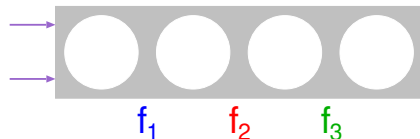
Focal length of a compound lens



Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length, f

$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f} \quad \longrightarrow \quad \frac{1}{i} = \frac{1}{f} - \frac{1}{o}$$

Focal length of a compound lens

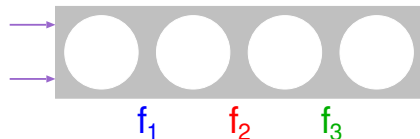


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$$\frac{1}{i_1} = \frac{1}{f_1} - \frac{1}{o_1}$$

Focal length of a compound lens



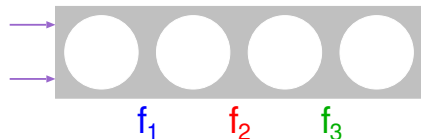
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$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f} \longrightarrow \frac{1}{i} = \frac{1}{f} - \frac{1}{o}$$

$$f_1 = f, o_1 = \infty$$

$$\frac{1}{i_1} = \frac{1}{f_1} - \frac{1}{o_1} \longrightarrow \frac{1}{i_1} = \frac{1}{f}$$

Focal length of a compound lens



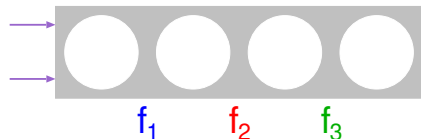
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Focal length of a compound lens



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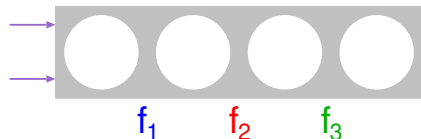
$$\frac{1}{i_2} = \frac{1}{f_2} - \frac{1}{o_2}$$

Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length, f

$$f_1 = f, o_1 = \infty$$

for the second lens, the image i_1 is a virtual object, $o_2 = -i_1$

Focal length of a compound lens



$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f} \rightarrow \frac{1}{i} = \frac{1}{f} - \frac{1}{o}$$

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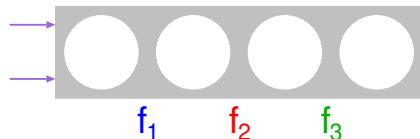
$$\frac{1}{i_2} = \frac{1}{f_2} - \frac{1}{o_2} \rightarrow \frac{1}{i_2} = \frac{1}{f} + \frac{1}{f}$$

Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length, f

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$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f} \rightarrow \frac{1}{i} = \frac{1}{f} - \frac{1}{o}$$

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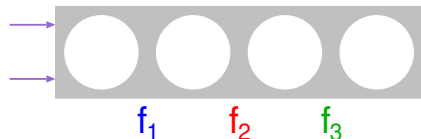
$$\frac{1}{i_2} = \frac{1}{f_2} - \frac{1}{o_2} \rightarrow \frac{1}{i_2} = \frac{1}{f} + \frac{1}{f} \rightarrow i_2 = \frac{f}{2}$$

Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length, f

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Focal length of a compound lens



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$$\frac{1}{i_2} = \frac{1}{f_2} - \frac{1}{o_2}$$

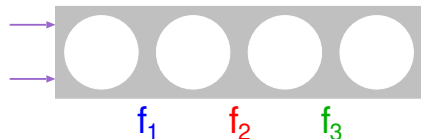
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similarly for the third lens, $o_3 = -i_2$

Focal length of a compound lens



$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f} \longrightarrow \frac{1}{i} = \frac{1}{f} - \frac{1}{o}$$

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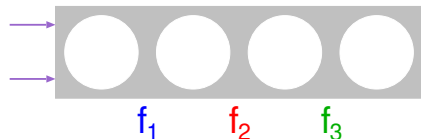
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$$\frac{1}{i_2} = \frac{1}{f_2} - \frac{1}{o_2} \rightarrow \frac{1}{i_2} = \frac{1}{f} + \frac{2}{f} \rightarrow i_2 = \frac{f}{3}$$

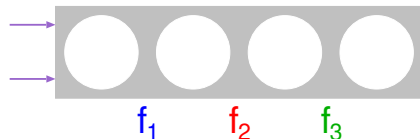
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Focal length of a compound lens



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Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length, f

$$f_1 = f, o_1 = \infty$$

for the second lens, the image i_1 is a virtual object, $o_2 = -i_1$

similarly for the third lens, $o_3 = -i_2$

so for N lenses $f_{\text{eff}} = f/N$

Rephasing distance



A spherical surface is not the ideal lens as it introduces aberrations. Derive the ideal shape for perfect focusing of x-rays.

Rephasing distance



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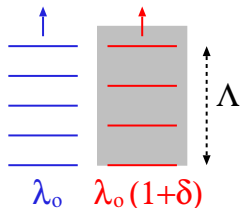
consider two waves, one traveling inside the solid and the other in vacuum,

$$\lambda = \lambda_0 / (1 - \delta) \approx \lambda_0 (1 + \delta)$$

Rephasing distance



A spherical surface is not the ideal lens as it introduces aberrations. Derive the ideal shape for perfect focusing of x-rays.



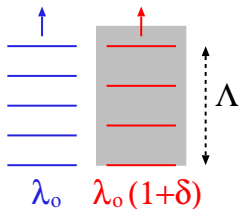
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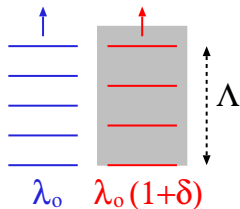
if the two waves start in phase, they will be in phase once again after a distance

$$\Lambda = (N + 1)\lambda_0 = N\lambda_0(1 + \delta)$$

Rephasing distance



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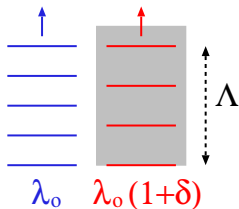
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$$N\lambda_0 + \lambda_0 = N\lambda_0 + N\delta\lambda_0$$

Rephasing distance



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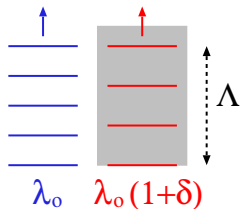
$$\Lambda = (N + 1)\lambda_0 = N\lambda_0(1 + \delta)$$

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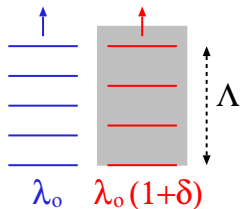
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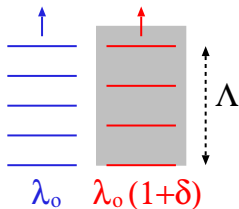
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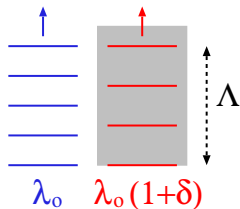
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$$\Lambda = N\lambda_0 = \frac{\lambda_0}{\delta} = \frac{2\pi}{\lambda_0 r_0 \rho}$$

Rephasing distance



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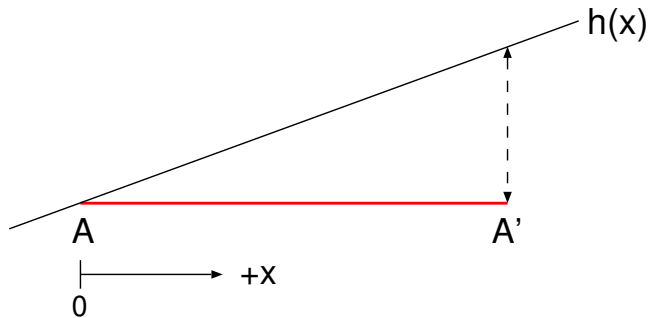
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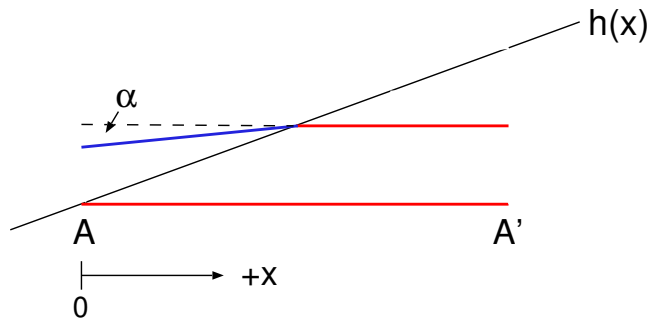
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$$\Lambda = N\lambda_0 = \frac{\lambda_0}{\delta} = \frac{2\pi}{\lambda_0 r_0 \rho} \approx 10 \mu\text{m}$$

Ideal interface profile - “thin” lens

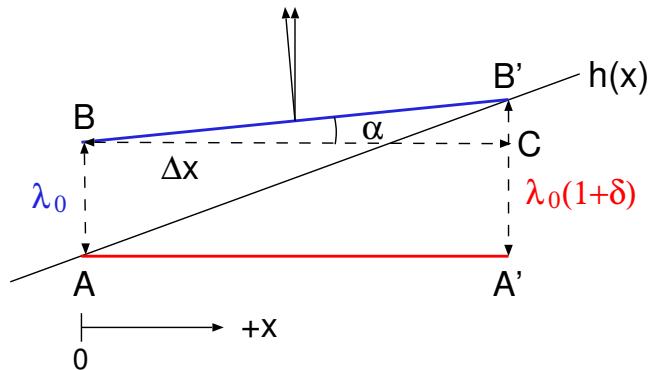


Ideal interface profile - “thin” lens



The wave exits the material into vacuum through a surface of profile $h(x)$, and is twisted by an angle α .

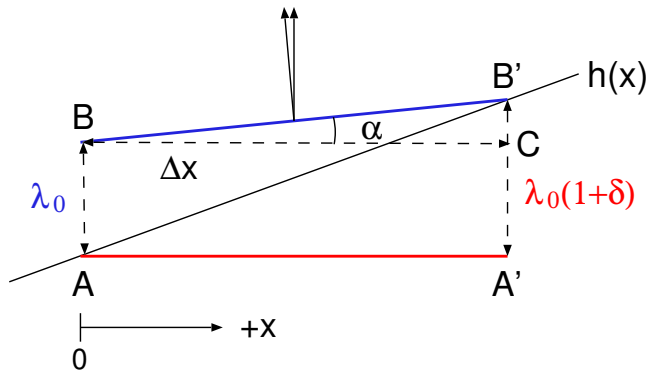
Ideal interface profile - “thin” lens



The wave exits the material into vacuum through a surface of profile $h(x)$, and is twisted by an angle α .

Follow the path of two points on the wavefront, A and A' as they propagate to B and B' .

Ideal interface profile - “thin” lens

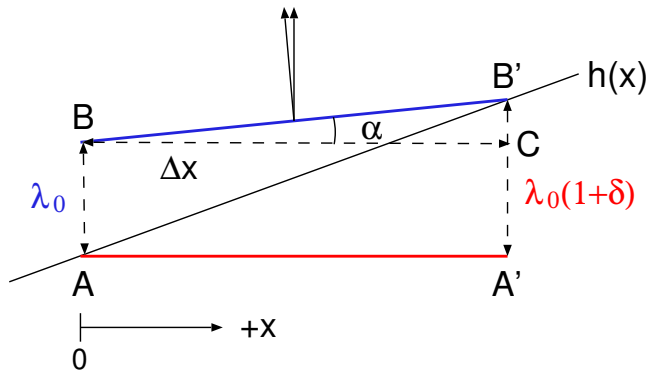


from the $AA'B'$ triangle

The wave exits the material into vacuum through a surface of profile $h(x)$, and is twisted by an angle α .

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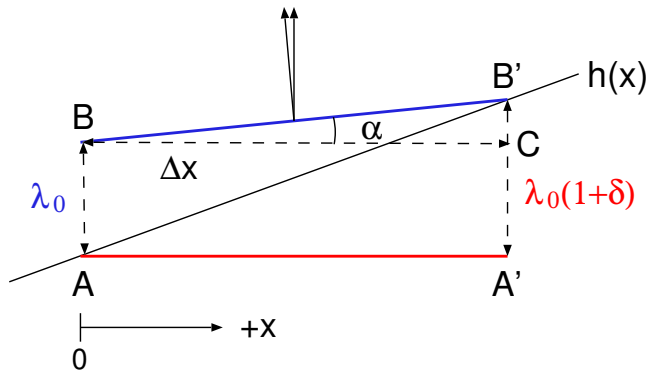
The wave exits the material into vacuum through a surface of profile $h(x)$, and is twisted by an angle α .

Follow the path of two points on the wavefront, A and A' as they propagate to B and B' .

from the $AA'B'$ triangle

$$\lambda_0(1 + \delta) = h'(x)\Delta x$$

Ideal interface profile - “thin” lens



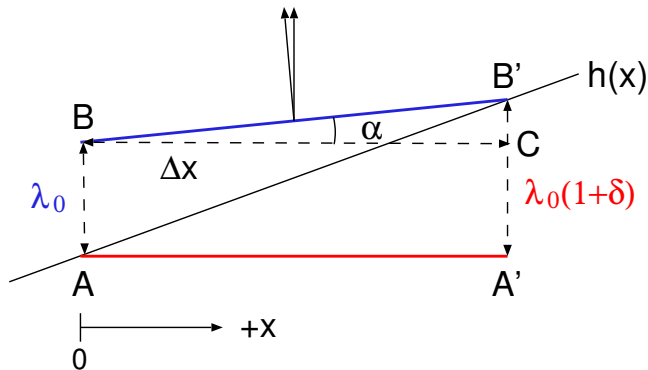
The wave exits the material into vacuum through a surface of profile $h(x)$, and is twisted by an angle α .

Follow the path of two points on the wavefront, A and A' as they propagate to B and B' .

from the $AA'B'$ triangle

$$\lambda_0(1 + \delta) = h'(x)\Delta x \longrightarrow \Delta x \approx \frac{\lambda_0}{h'(x)}$$

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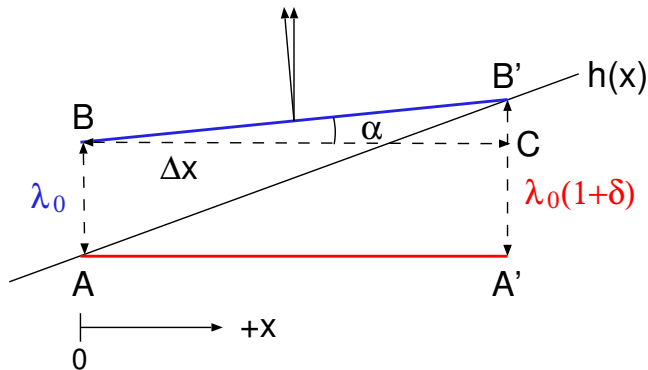
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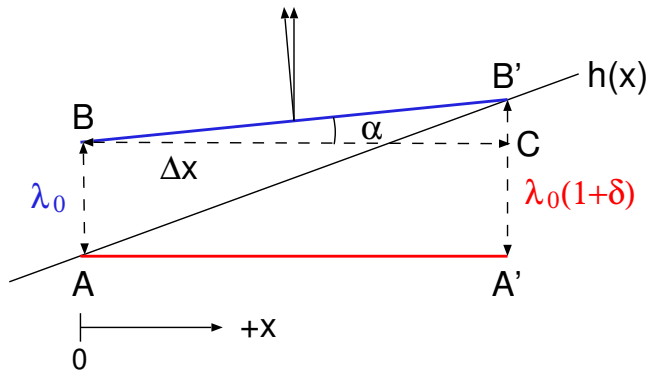
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$$\lambda_0 (1 + \delta) = h'(x) \Delta x \longrightarrow \Delta x \approx \frac{\lambda_0}{h'(x)}$$

$$\alpha(x) \approx \frac{\lambda_0 \delta}{\Delta x}$$

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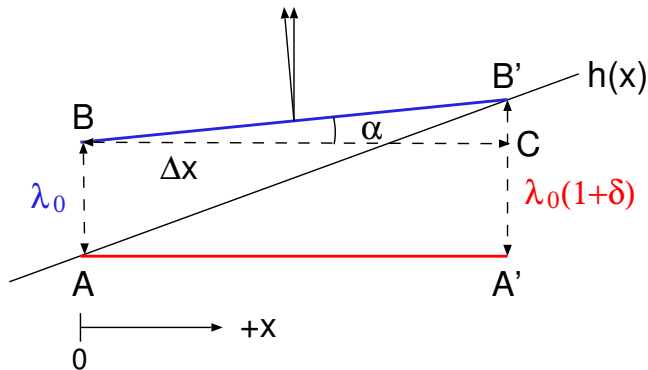
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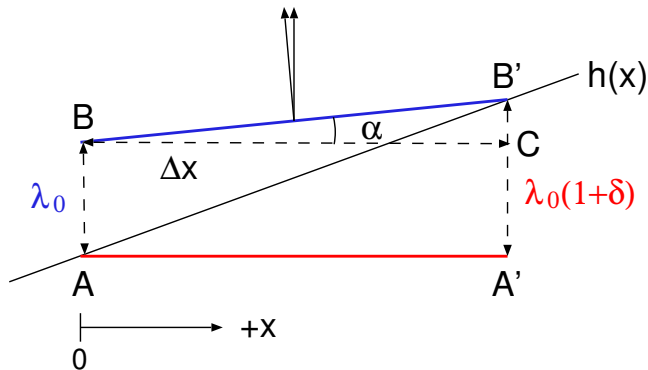
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from the $AA'B'$ triangle
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using $\Lambda = \lambda_0/\delta$

$$\lambda_0(1 + \delta) = h'(x)\Delta x \longrightarrow \Delta x \approx \frac{\lambda_0}{h'(x)}$$

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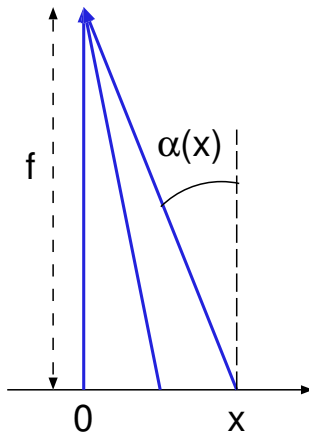
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Ideal interface profile - “thin” lens

If the desired focal length of this lens is f , the wave must be redirected at an angle which depends on the distance from the optical axis

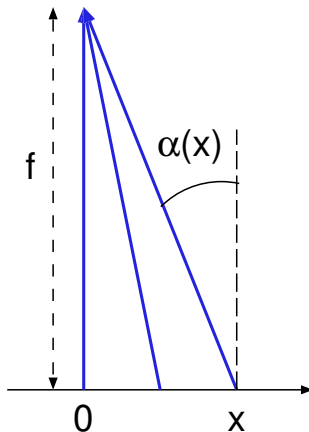


Ideal interface profile - “thin” lens



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Ideal interface profile - “thin” lens

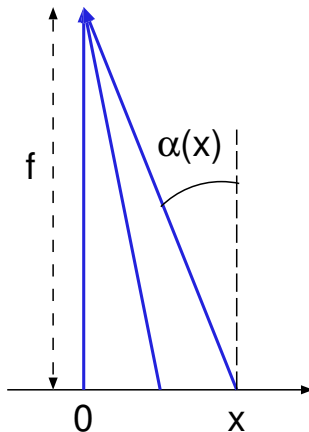


If the desired focal length of this lens is f , the wave must be redirected at an angle which depends on the distance from the optical axis

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$$\frac{\lambda_0 h'(x)}{\Lambda} = \frac{x}{f}$$



Ideal interface profile - “thin” lens

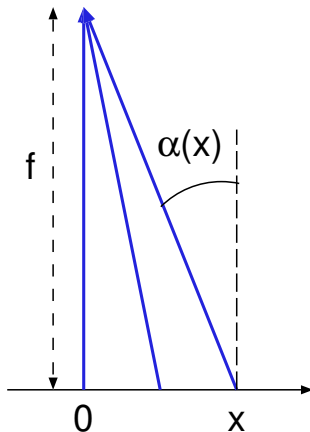


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Ideal interface profile - “thin” lens



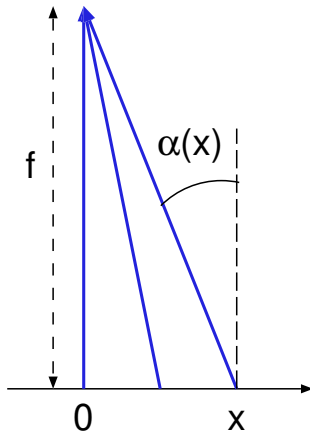
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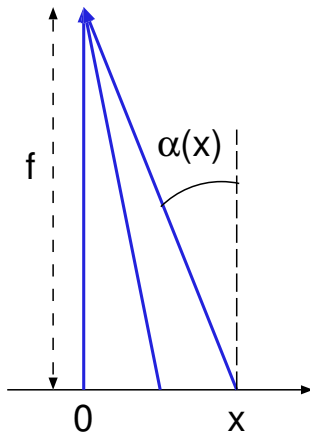
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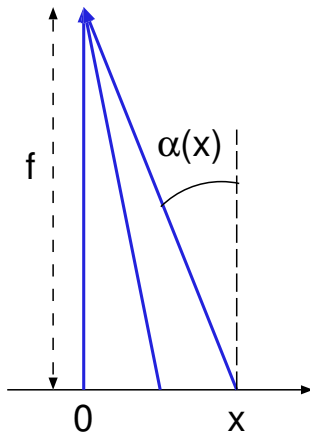
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$$\frac{h(x)}{\Lambda} = \frac{x^2}{2f \lambda_0} = \left[\frac{x}{\sqrt{2f \lambda_0}} \right]^2$$



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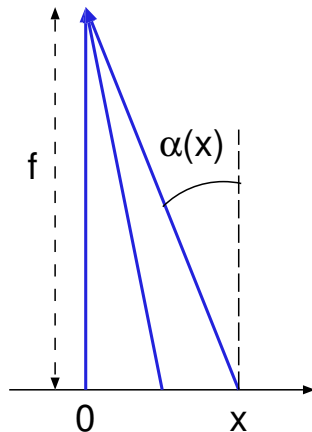
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a parabola is the ideal surface shape for focusing by refraction for a “thin” lens with limited aperture

Focal length of circular lens



From the previous expression for the ideal parabolic surface, the focal length can be written in terms of the surface profile.

Focal length of circular lens



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$$f = \frac{x^2 \Lambda}{2\lambda_0 h(x)}$$

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$$f = \frac{x^2 \Lambda}{2\lambda_0 h(x)} = \frac{1}{2\delta} \frac{x^2}{h(x)}$$

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if the surface is a circle instead of a parabola

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confining the aperture to values where
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$$\begin{aligned} h(x) &= R - \sqrt{R^2 - x^2} = R - R\sqrt{1 - \frac{x^2}{R^2}} \\ &\approx R - R\left(1 - \frac{1}{2} \frac{x^2}{R^2}\right) \approx \frac{x^2}{2R} \\ f &\approx \frac{R}{\delta} \end{aligned}$$

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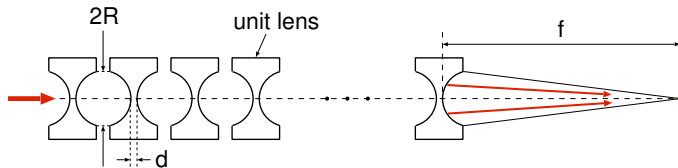
and thus the focal length becomes

$$f \approx \frac{R}{\delta}$$

for $2N$ circular lenses we have

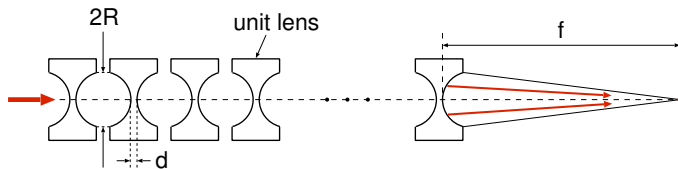
$$f_{2N} \approx \frac{R}{2N\delta}$$

Focussing by a beryllium lens



H.R. Beguiristain et al., "X-ray focusing with compound lenses made from beryllium," *Optics Lett.*, **27**, 778 (2007).

Focussing by a beryllium lens

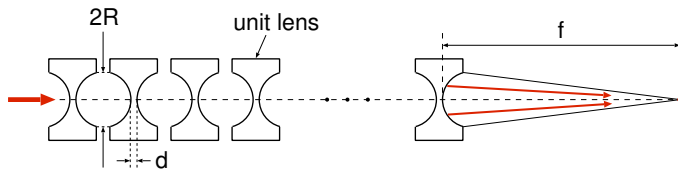


For 50 holes of radius $R = 1\text{mm}$ in beryllium (Be) at $E = 10\text{keV}$, we can calculate the focal length, knowing $\delta = 3.41 \times 10^{-6}$

$$f_N = \frac{R}{2N\delta}$$

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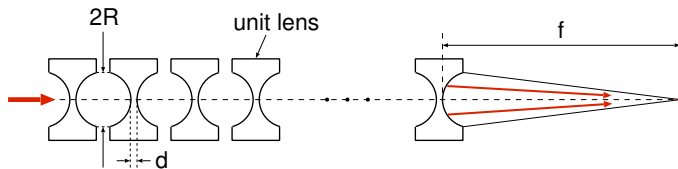


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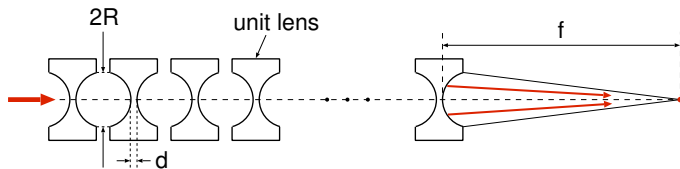


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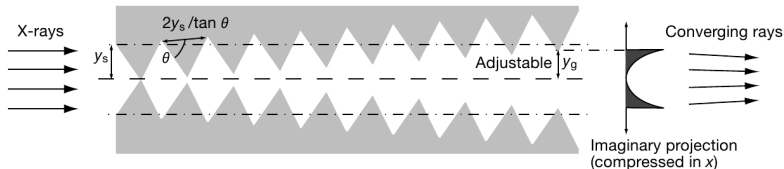
depending on the wall thickness of the lenslets, the transmission can be up to 74%

H.R. Beguiristain et al., "X-ray focusing with compound lenses made from beryllium," *Optics Lett.*, **27**, 778 (2007).

Alligator-type lenses



Perhaps one of the most original x-ray lenses has been made by using old vinyl records in an “alligator” configuration.

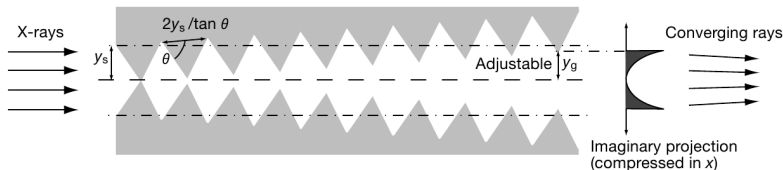


Björn Cederström et al., “Focusing hard X-rays with old LPs”, *Nature* **404**, 951 (2000).

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This design has also been used to make lenses out of lithium metal.

E.M. Dufresne et al., “Lithium metal for x-ray refractive optics”, *Appl. Phys. Lett.* **79**, 4085 (2001).

Extruded Al lens



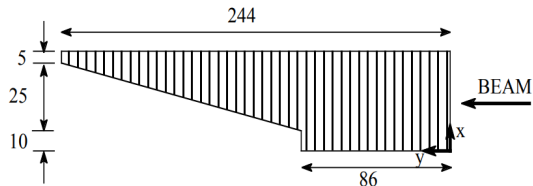
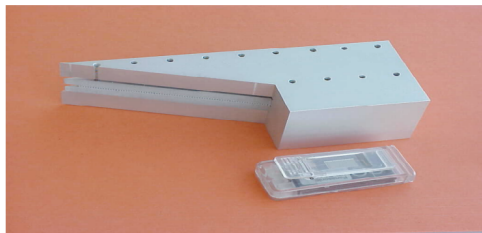
The compound refractive lenses (CRL) are useful for fixed focus but are difficult to use if a variable focal distance and a long focal length is required.

A. Khounsary et al., "Fabrication, testing, and performance of a variable focus x-ray compound lens", *Proc. SPIE* **4783**, 49-54 (2002).

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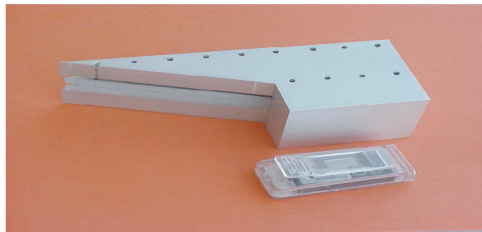


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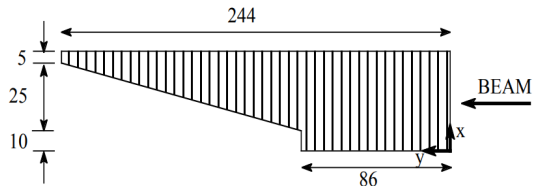
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Extruded aluminum lens with parabolic figure

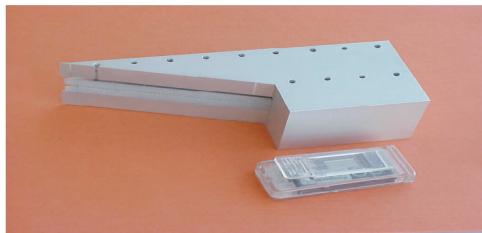


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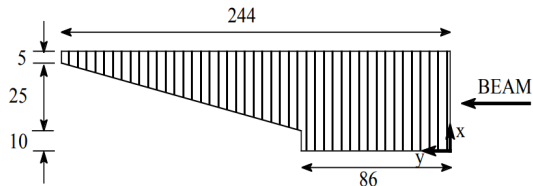


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Extruded aluminum lens with parabolic figure

Cut diagonally to expose variable number of "lenses" to a horizontal beam

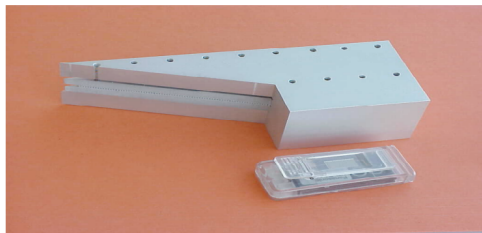


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Extruded Al lens



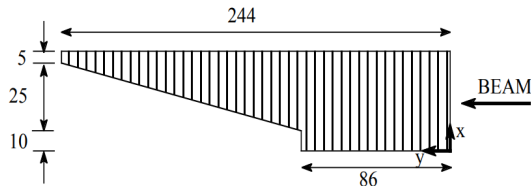
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Cut diagonally to expose variable number of “lenses” to a horizontal beam

Horizontal translation allows change in focal length but it is quantized, not continuous



A. Khounsary et al., “Fabrication, testing, and performance of a variable focus x-ray compound lens”, *Proc. SPIE* **4783**, 49-54 (2002).

Variable focal length CRL



A continuously variable focal length is very important for two specific reasons: tracking sample position, and keeping the focal length constant as energy is changed.

Variable focal length CRL



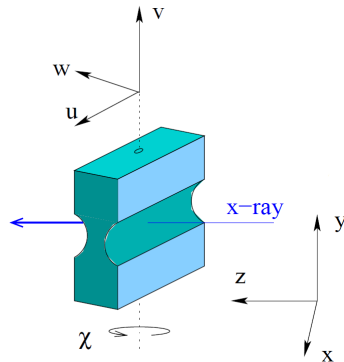
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A continuously variable focal length is very important for two specific reasons: tracking sample position, and keeping the focal length constant as energy is changed. This can be achieved with a rotating lens system

Start with a 2 hole CRL.



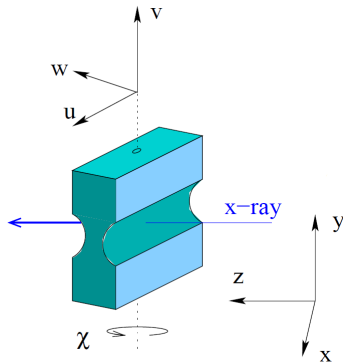
B. Adams and C. Rose-Petruck, "X-ray focusing scheme with continuously variable lens," *J. Synchrotron Radiation* **22**, 16-22 (2015).

Variable focal length CRL



A continuously variable focal length is very important for two specific reasons: tracking sample position, and keeping the focal length constant as energy is changed. This can be achieved with a rotating lens system

Start with a 2 hole CRL. Rotate by an angle χ about vertical axis



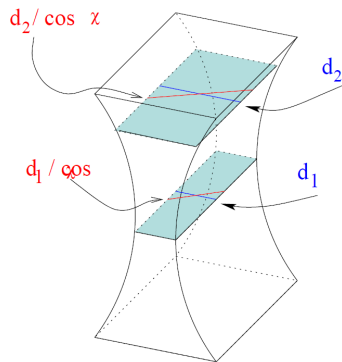
B. Adams and C. Rose-Petruck, "X-ray focusing scheme with continuously variable lens," *J. Synchrotron Radiation* **22**, 16-22 (2015).

Variable focal length CRL



A continuously variable focal length is very important for two specific reasons: tracking sample position, and keeping the focal length constant as energy is changed. This can be achieved with a rotating lens system

Start with a 2 hole CRL. Rotate by an angle χ about vertical axis giving an effective change in the number of “lenses” by a factor $1/\cos \chi$.



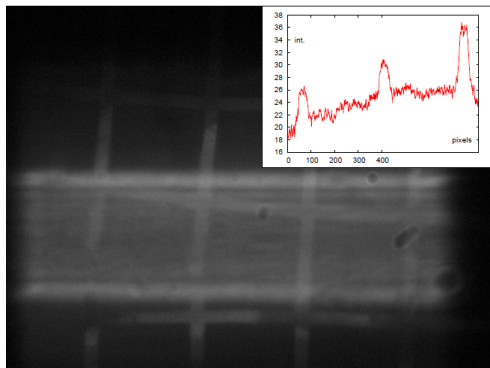
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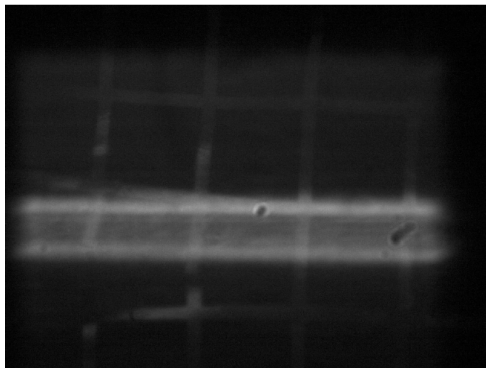


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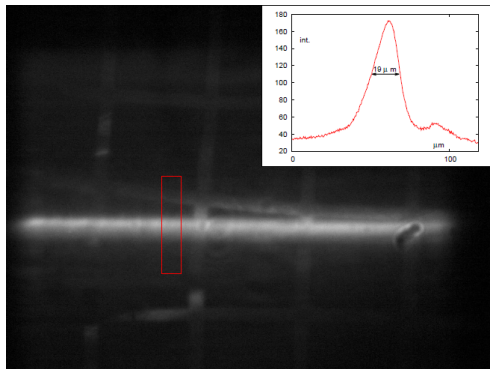
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At $\chi = 30^\circ$, it is under $50\mu\text{m}$

Optimal focus is $20\mu\text{m}$ at $\chi = 40^\circ$



Polycapillary optics



A polycapillary is a focusing optic made up of an array of thousands of thin-walled hollow tubes which are $> 65\%$ empty space

F.A. Hofmann et al., "Focusing of synchrotron radiation with polycapillary optics,"
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They rely on total external reflection to guide x-rays through the capillary to a final focus with gains per unit area of up to ~ 1000

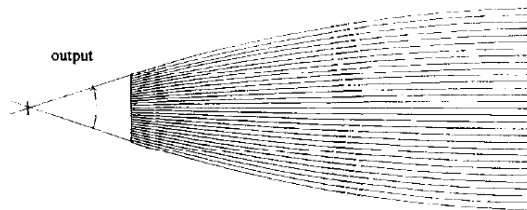
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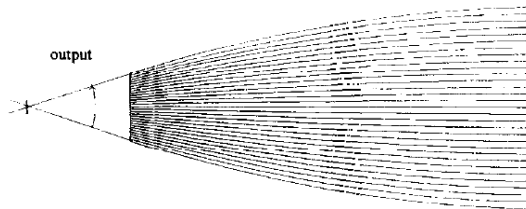
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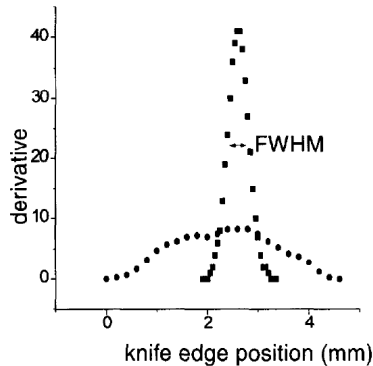


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Improving polycapillary optic performance



One drawback of a glass capillary is that the transmission at high energies is reduced because of critical angle restrictions

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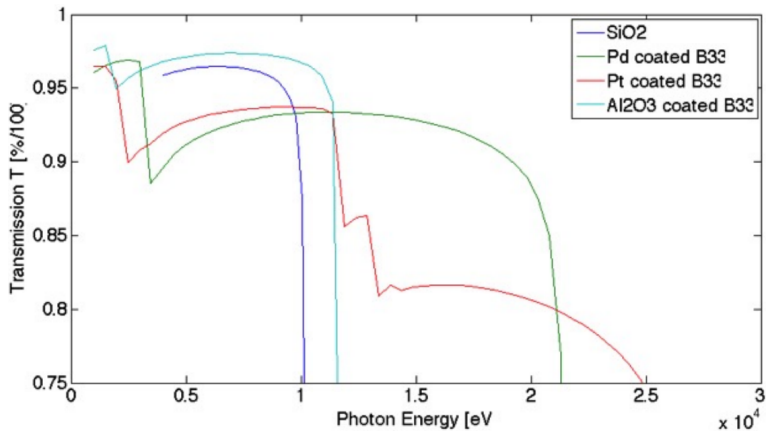
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Elliptical lens surface



In calculating the optimal surface profile for a refractive lens, an important approximation was made which resulted in a parabolic surface

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What happens if we lift this restriction?

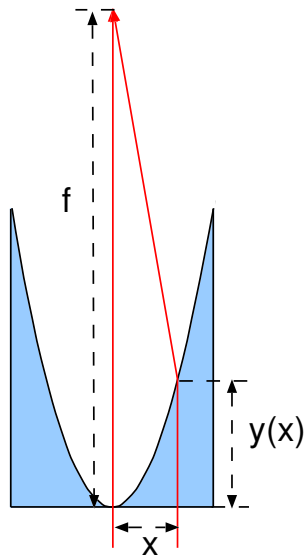
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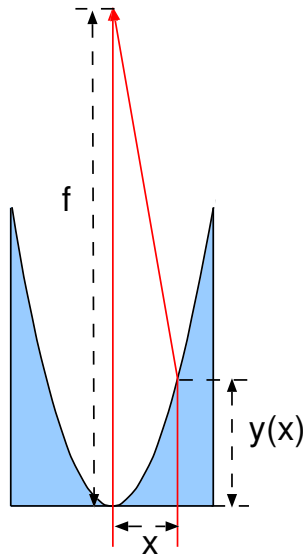


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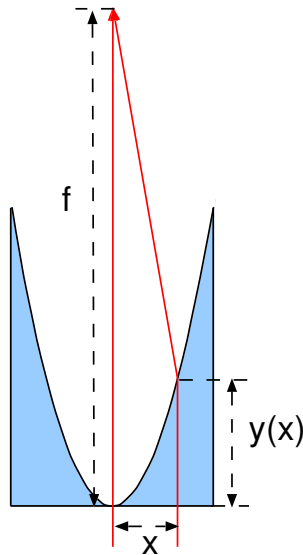
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$$f = y(1 - \delta) + \sqrt{(f - y)^2 + x^2}$$



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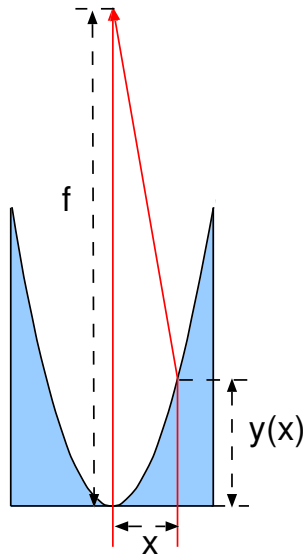
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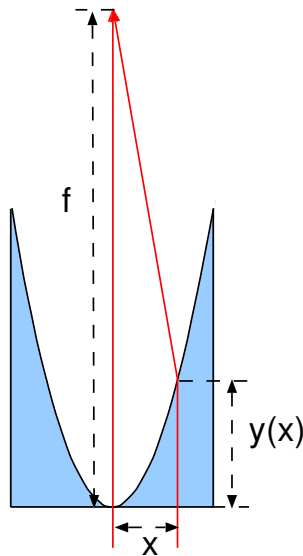
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$$(f - y + \delta y)^2 = (f - y)^2 + x^2$$

$$2f\delta y - (2\delta - \delta^2)y^2 = x^2$$



Elliptical lens surface



Ideal surface

Ellipse

Elliptical lens surface



Ideal surface

$$0 = x^2 + (2\delta - \delta^2)y^2 - 2f\delta y$$

Ellipse

$$1 = \frac{x^2}{a^2} + \frac{(y - b)^2}{b^2}$$

Elliptical lens surface



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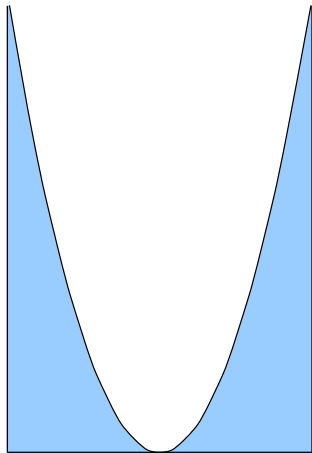
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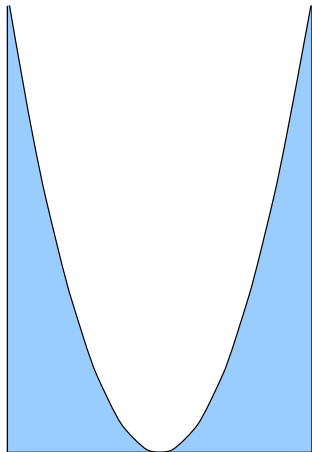
The ideal surface for a thick lens is an ellipse

How to make a Fresnel lens



The ideal refracting lens has an elliptical shape but this is impractical to make. Assuming the parabolic approximation:

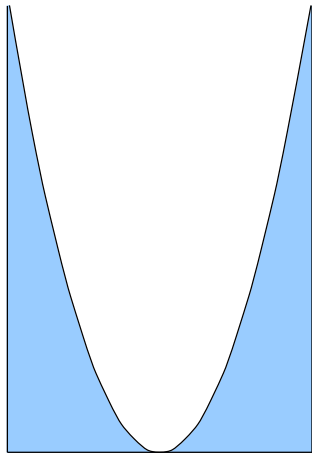
How to make a Fresnel lens



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$$h(x) = \Lambda \left(\frac{x}{\sqrt{2\lambda_o f}} \right)^2$$

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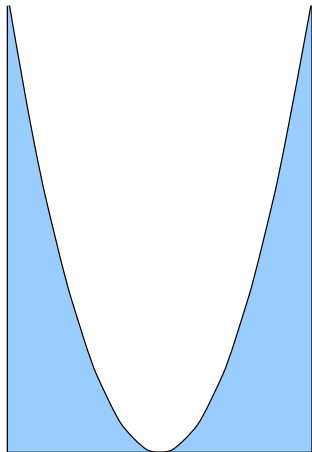


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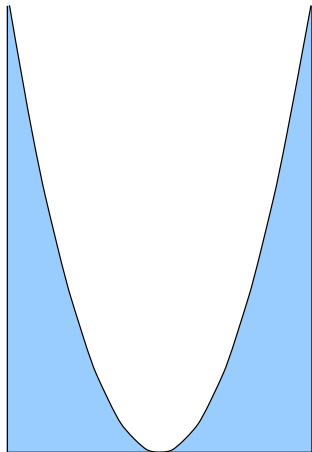
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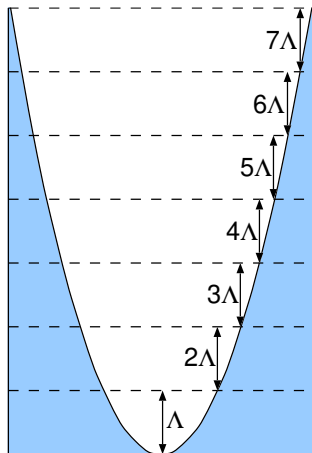
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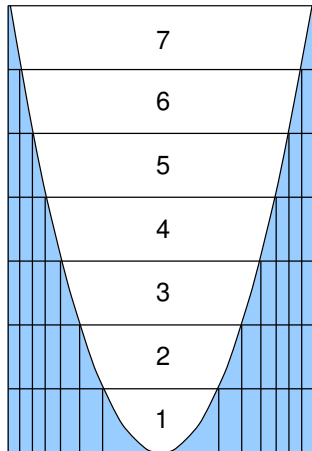
aspect ratio too large for a stable structure and absorption would be too large!

How to make a Fresnel lens



Mark off the longitudinal zones (of thickness Λ) where the waves inside and outside the material are in phase.

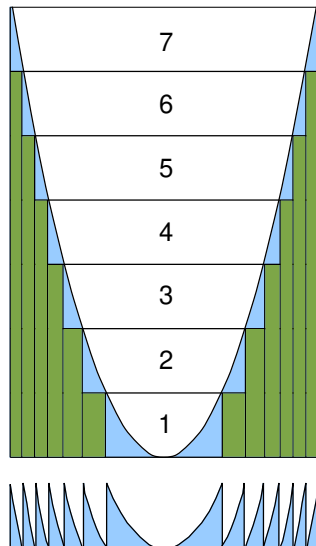
How to make a Fresnel lens



Mark off the longitudinal zones (of thickness Λ) where the waves inside and outside the material are in phase.

Each block of thickness Λ serves no purpose for refraction but only attenuates the wave.

How to make a Fresnel lens

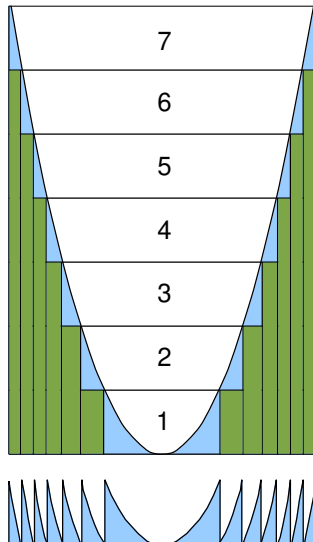


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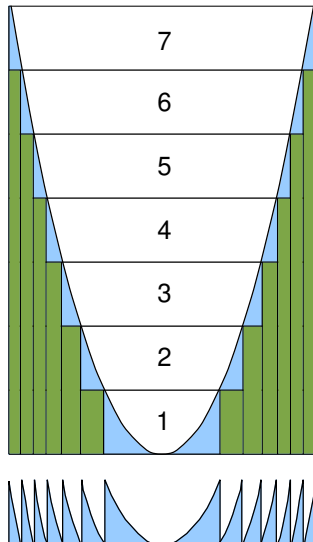
This material can be removed and the remaining material collapsed to produce a Fresnel lens which has the same optical properties as the parabolic lens as long as $f \gg N\Lambda$ where N is the number of zones.

Fresnel lens dimensions



The outermost zones become very small and thus limit the overall aperture of the zone plate. The dimensions of outermost zone, N can be calculated by first defining a scaled height and lateral dimension

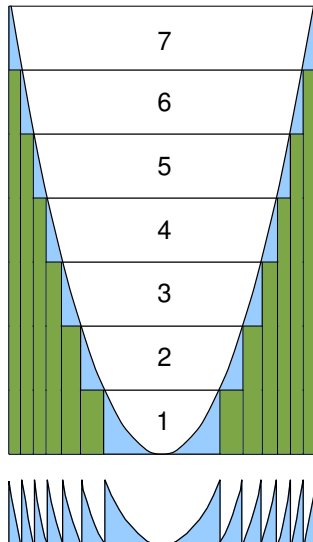
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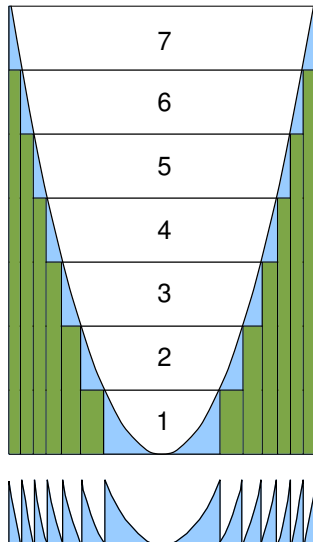
$$\nu = \frac{h(x)}{\Lambda}$$

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$$\nu = \frac{h(x)}{\Lambda} \quad \xi = \frac{x}{\sqrt{2\lambda_o f}}$$

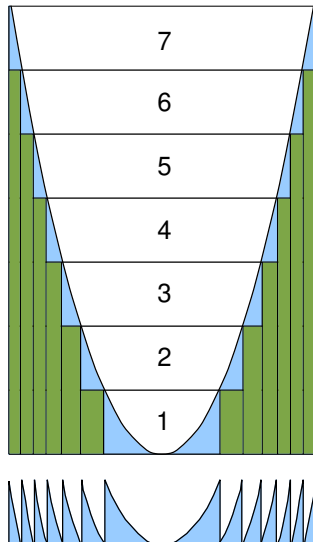


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Since $\nu = \xi^2$, the position of the N^{th} zone is $\xi_N = \sqrt{N}$ and the scaled width of the N^{th} (outermost) zone is

Fresnel lens dimensions



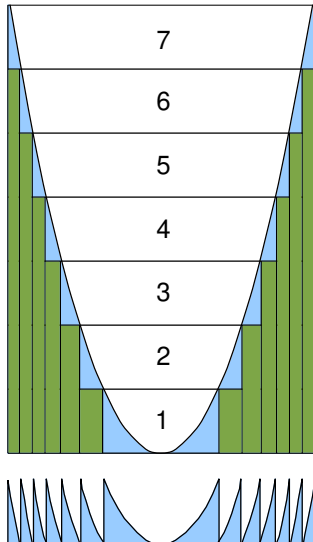
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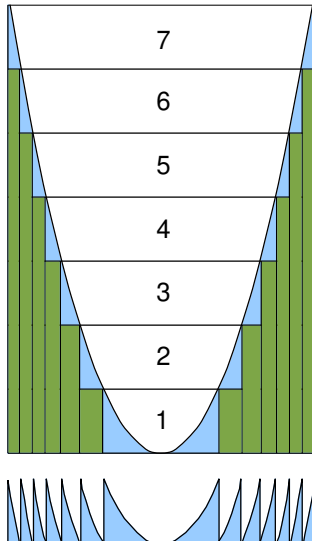
$$\Delta\xi_N = \xi_N - \xi_{N-1} = \sqrt{N} - \sqrt{N-1}$$

Fresnel lens dimensions



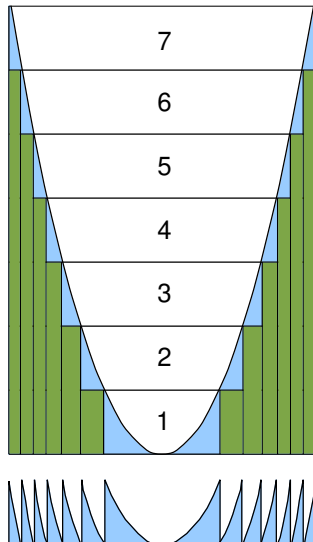
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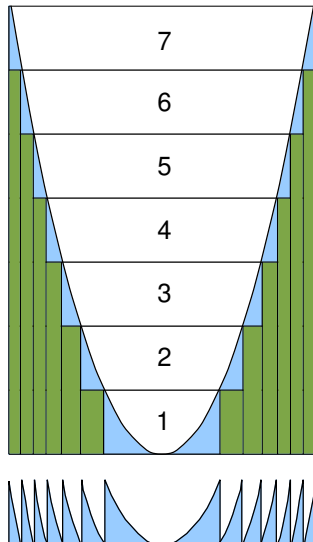
$$\begin{aligned}\Delta\xi_N &= \xi_N - \xi_{N-1} = \sqrt{N} - \sqrt{N-1} \\ &= \sqrt{N} \left(1 - \sqrt{1 - \frac{1}{N}} \right)\end{aligned}$$

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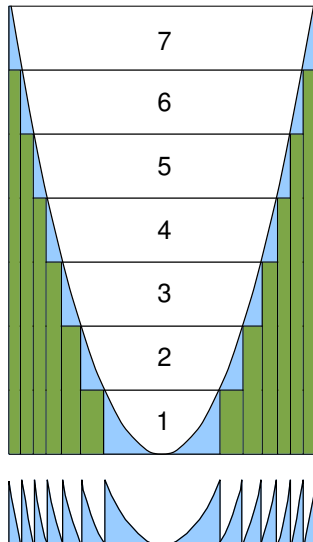
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The diameter of the entire lens is thus

$$2\xi_N = 2\sqrt{N} = \frac{1}{\Delta\xi_N}$$

Fresnel lens example



In terms of the unscaled variables

$$\Delta x_N = \Delta \xi_N \sqrt{2\lambda_o f}$$

Fresnel lens example



In terms of the unscaled variables

$$\Delta x_N = \Delta \xi_N \sqrt{2\lambda_o f} = \sqrt{\frac{\lambda_o f}{2N}}$$

Fresnel lens example



In terms of the unscaled variables

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$$d_N = 2\xi_N$$

Fresnel lens example



In terms of the unscaled variables

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$$d_N = 2\xi_N = \frac{\sqrt{2\lambda_o f}}{\Delta \xi_N}$$

Fresnel lens example



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If we take

$$\lambda_o = 1\text{\AA} = 1 \times 10^{-10}\text{m}$$

$$f = 50\text{cm} = 0.5\text{m}$$

$$N = 100$$

Fresnel lens example



In terms of the unscaled variables

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If we take

$$\lambda_o = 1\text{\AA} = 1 \times 10^{-10}\text{m}$$

$$f = 50\text{cm} = 0.5\text{m}$$

$$N = 100$$

$$\Delta x_N = 5 \times 10^{-7}\text{m} = 500\text{nm}$$

Fresnel lens example



In terms of the unscaled variables

$$\Delta x_N = \Delta \xi_N \sqrt{2\lambda_o f} = \sqrt{\frac{\lambda_o f}{2N}}$$

$$d_N = 2\xi_N = \frac{\sqrt{2\lambda_o f}}{\Delta \xi_N} = 2\sqrt{N} \sqrt{2\lambda_o f} = \sqrt{2N\lambda_o f}$$

If we take

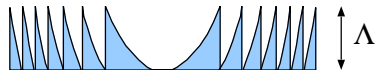
$$\lambda_o = 1\text{\AA} = 1 \times 10^{-10}\text{m}$$

$$f = 50\text{cm} = 0.5\text{m}$$

$$N = 100$$

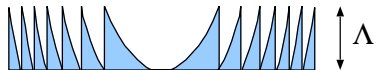
$$\Delta x_N = 5 \times 10^{-7}\text{m} = 500\text{nm} \qquad d_N = 2 \times 10^{-4}\text{m} = 100\mu\text{m}$$

Making a Fresnel zone plate

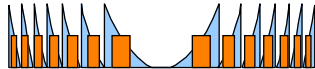


The specific shape required for a zone plate is difficult to fabricate, consequently, it is convenient to approximate the nearly triangular zones with a rectangular profile.

Making a Fresnel zone plate

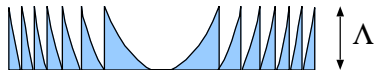


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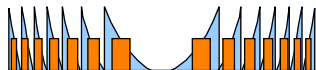


In practice, since the outermost zones are very small, zone plates are generally fabricated as alternating zones (rings for 2D) of materials with a large Z-contrast, such as Au/Si or W/C.

Making a Fresnel zone plate



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This kind of zone plate is not as efficient as a true Fresnel lens would be in the x-ray regime. Nevertheless, efficiencies up to 35% have been achieved.

Zone plate fabrication



Making high aspect ratio zone plates is challenging but a new process has been developed to make plates with an aspect ratio as high as 25.

M. Wojcik et al., "X-ray zone plates with 25 aspect ratio using a 2- μm -thick ultranocrystalline diamond mold," *Microsyst. Technol.* **20**, 2045-2050 (2014).

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Start with Ultra nano crystalline diamond (UNCD) films on SiN.

UNCD

SiN



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Start with Ultra nano crystalline diamond (UNCD) films on SiN. Coat with hydrogen silsesquioxane (HSQ).

HSQ
UNCD
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HSQ
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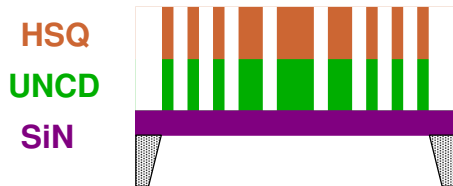
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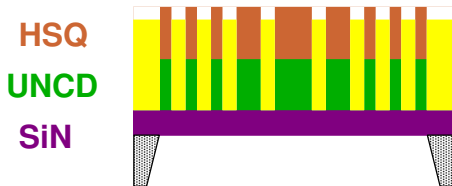
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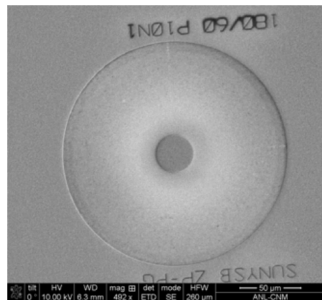
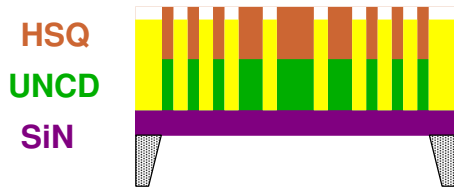
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The whole 150nm diameter zone plate



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Zone plate fabrication

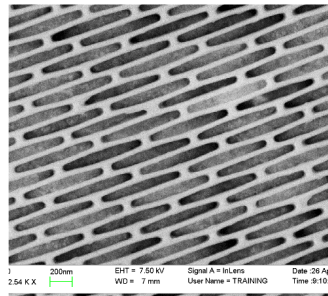
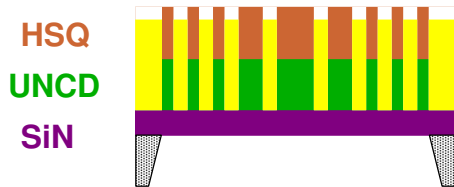


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Detail view of outer zones



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