

# Today's outline - January 30, 2020

# Today's outline - January 30, 2020

- HW #2

# Today's outline - January 30, 2020

- HW #2
- Area detectors

# Today's outline - January 30, 2020

- HW #2
- Area detectors
- Refraction and reflection

## Today's outline - January 30, 2020

- HW #2
- Area detectors
- Refraction and reflection
- Boundary conditions at an interface

## Today's outline - January 30, 2020

- HW #2
- Area detectors
- Refraction and reflection
- Boundary conditions at an interface
- The Fresnel equations

# Today's outline - January 30, 2020

- HW #2
- Area detectors
- Refraction and reflection
- Boundary conditions at an interface
- The Fresnel equations
- Reflectivity and Transmittivity

# Today's outline - January 30, 2020

- HW #2
- Area detectors
- Refraction and reflection
- Boundary conditions at an interface
- The Fresnel equations
- Reflectivity and Transmittivity
- Normalized  $q$ -coordinates



# Today's outline - January 30, 2020

- HW #2
- Area detectors
- Refraction and reflection
- Boundary conditions at an interface
- The Fresnel equations
- Reflectivity and Transmittivity
- Normalized  $q$ -coordinates

Reading Assignment: Chapter 3.4

# Today's outline - January 30, 2020

- HW #2
- Area detectors
- Refraction and reflection
- Boundary conditions at an interface
- The Fresnel equations
- Reflectivity and Transmittivity
- Normalized  $q$ -coordinates

Reading Assignment: Chapter 3.4

Homework Assignment #02:

Problems to be provided

due Tuesday, February 18, 2020

## HW #02

1. Knowing that the photoelectric absorption of an element scales as the inverse of the energy cubed, calculate:
  - (a) the absorption coefficient at 10keV for copper when the value at 5keV is  $1698.3 \text{ cm}^{-1}$ ;
  - (b) The actual absorption coefficient of copper at 10keV is  $1942.1 \text{ cm}^{-1}$ , why is this so different than your calculated value?
2. A 30 cm long, ionization chamber, filled with 80% helium and 20% nitrogen gases at 1 atmosphere, is being used to measure the photon rate (photons/sec) in a synchrotron beamline at 12 keV. If a current of 10 nA is measured, what is the photon flux entering the ionization chamber?
3. A 5 cm deep ionization chamber is used to measure the fluorescence from a sample containing arsenic (As). Using any noble gases or nitrogen, determine a gas fill (at 1 atmosphere) for this chamber which absorbs at least 60% of the incident photons. How does this change if you are measuring the fluorescence from ruthenium (Ru)?

## HW #02

4. Calculate the critical angle of reflection of 10 keV and 30 keV x-rays for:

- (a) A slab of glass ( $\text{SiO}_2$ );
- (b) A thick chromium mirror;
- (c) A thick platinum mirror.
- (d) If the incident x-ray beam is 2 mm high, what length of mirror is required to reflect the entire beam for each material?

5. Calculate the fraction of silver (Ag) fluorescence x-rays which are absorbed in a 1 mm thick silicon (Si) detector and the charge pulse expected for each absorbed photon. Repeat the calculation for a 1 mm thick germanium (Ge) detector.

# Area detectors

Area detectors have been used for many years and include older technologies such as 2D gas proportional detectors, image plates, and even photographic film!

## Area detectors

Area detectors have been used for many years and include older technologies such as 2D gas proportional detectors, image plates, and even photographic film!

Will look carefully only at more modern technologies such as Charge Coupled Device (CCD) based detectors and active pixel array detectors

## Area detectors

Area detectors have been used for many years and include older technologies such as 2D gas proportional detectors, image plates, and even photographic film!

Will look carefully only at more modern technologies such as Charge Coupled Device (CCD) based detectors and active pixel array detectors

The basic criteria which need to be evaluated in order to choose the ideal detector for an experiment are:

# Area detectors

Area detectors have been used for many years and include older technologies such as 2D gas proportional detectors, image plates, and even photographic film!

Will look carefully only at more modern technologies such as Charge Coupled Device (CCD) based detectors and active pixel array detectors

The basic criteria which need to be evaluated in order to choose the ideal detector for an experiment are:

- Area -  $20\text{ cm} \times 20\text{ cm}$  is often standard



# Area detectors

Area detectors have been used for many years and include older technologies such as 2D gas proportional detectors, image plates, and even photographic film!

Will look carefully only at more modern technologies such as Charge Coupled Device (CCD) based detectors and active pixel array detectors

The basic criteria which need to be evaluated in order to choose the ideal detector for an experiment are:

- Area -  $20\text{ cm} \times 20\text{ cm}$  is often standard
- Pixel size -  $20\ \mu\text{m} \times 20\ \mu\text{m}$  or larger is typical

## Area detectors

Area detectors have been used for many years and include older technologies such as 2D gas proportional detectors, image plates, and even photographic film!

Will look carefully only at more modern technologies such as Charge Coupled Device (CCD) based detectors and active pixel array detectors

The basic criteria which need to be evaluated in order to choose the ideal detector for an experiment are:

- Area -  $20\text{ cm} \times 20\text{ cm}$  is often standard
- Pixel size -  $20\text{ }\mu\text{m} \times 20\text{ }\mu\text{m}$  or larger is typical
- Detector speed - readouts of 5 ms to 1 s are available

## Area detectors

Area detectors have been used for many years and include older technologies such as 2D gas proportional detectors, image plates, and even photographic film!

Will look carefully only at more modern technologies such as Charge Coupled Device (CCD) based detectors and active pixel array detectors

The basic criteria which need to be evaluated in order to choose the ideal detector for an experiment are:

- Area -  $20\text{ cm} \times 20\text{ cm}$  is often standard
- Pixel size -  $20\text{ }\mu\text{m} \times 20\text{ }\mu\text{m}$  or larger is typical
- Detector speed - readouts of 5 ms to 1 s are available
- Dynamic range - 16 bits is typical, more is possible

## Area detectors

Area detectors have been used for many years and include older technologies such as 2D gas proportional detectors, image plates, and even photographic film!

Will look carefully only at more modern technologies such as Charge Coupled Device (CCD) based detectors and active pixel array detectors

The basic criteria which need to be evaluated in order to choose the ideal detector for an experiment are:

- Area -  $20\text{ cm} \times 20\text{ cm}$  is often standard
- Pixel size -  $20\text{ }\mu\text{m} \times 20\text{ }\mu\text{m}$  or larger is typical
- Detector speed - readouts of 5 ms to 1 s are available
- Dynamic range - 16 bits is typical, more is possible

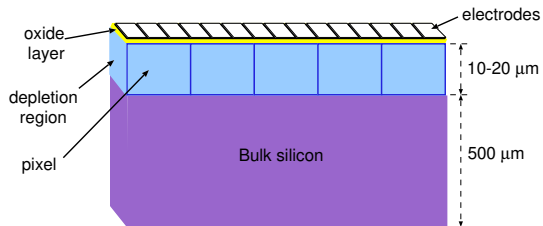
The most advanced detectors can easily cost over a million dollars!

## CCD detectors - direct

One of the two configurations typical of CCD detectors is direct measurement of x-rays

## CCD detectors - direct

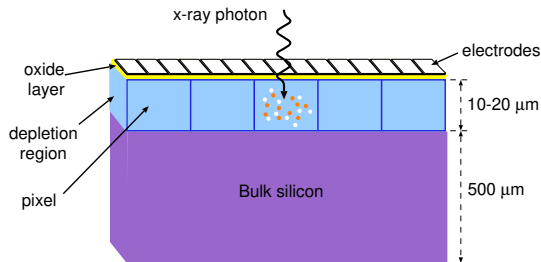
One of the two configurations typical of CCD detectors is direct measurement of x-rays



the direct measurement CCD is just a segmented silicon detector

## CCD detectors - direct

One of the two configurations typical of CCD detectors is direct measurement of x-rays

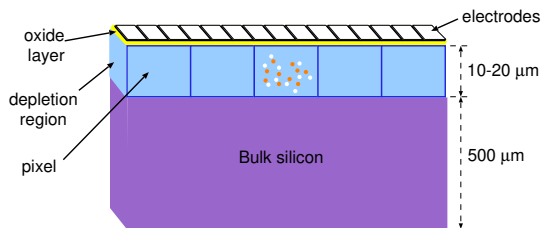


the direct measurement CCD is just a segmented silicon detector

the x-ray deposits its energy directly in the depletion region, creating electron-hole pairs

## CCD detectors - direct

One of the two configurations typical of CCD detectors is direct measurement of x-rays



the direct measurement CCD is just a segmented silicon detector

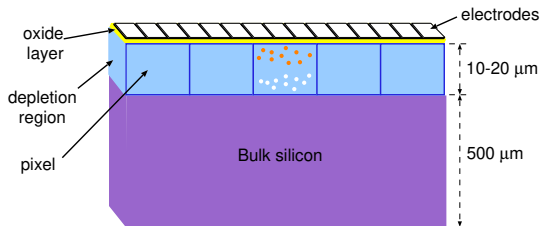
the x-ray deposits its energy directly in the depletion region, creating electron-hole pairs

the electrons and holes are trapped and accumulate during the exposure time



## CCD detectors - direct

One of the two configurations typical of CCD detectors is direct measurement of x-rays



when readout starts, the charge is swept to the electrodes and read out, consecutively, line-by-line

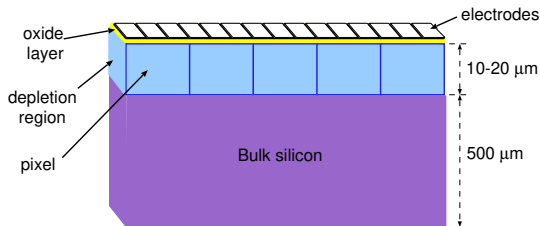
the direct measurement CCD is just a segmented silicon detector

the x-ray deposits its energy directly in the depletion region, creating electron-hole pairs

the electrons and holes are trapped and accumulate during the exposure time

## CCD detectors - direct

One of the two configurations typical of CCD detectors is direct measurement of x-rays



the direct measurement CCD is just a segmented silicon detector

the x-ray deposits its energy directly in the depletion region, creating electron-hole pairs

the electrons and holes are trapped and accumulate during the exposure time

when readout starts, the charge is swept to the electrodes and read out, consecutively, line-by-line

expensive to make very large, limited sensitivity to high energies

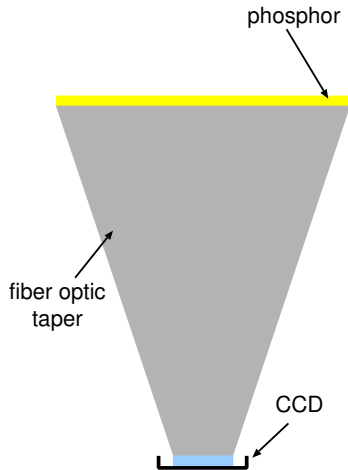
## CCD detectors - indirect

The largest area detectors are made using the CCD in indirect mode

## CCD detectors - indirect

The largest area detectors are made using the CCD in indirect mode

The CCD is coupled optically to a fiber optic taper which ends at a large phosphor

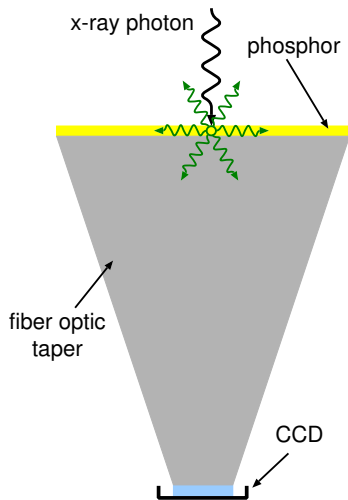


## CCD detectors - indirect

The largest area detectors are made using the CCD in indirect mode

The CCD is coupled optically to a fiber optic taper which ends at a large phosphor

When an x-ray is absorbed at the phosphor, visible light photons are emitted in all directions



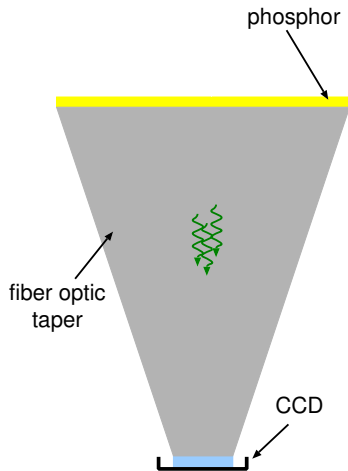
## CCD detectors - indirect

The largest area detectors are made using the CCD in indirect mode

The CCD is coupled optically to a fiber optic taper which ends at a large phosphor

When an x-ray is absorbed at the phosphor, visible light photons are emitted in all directions

A fraction of the visible light is guided to the CCD chip(s) at the end of the taper



## CCD detectors - indirect

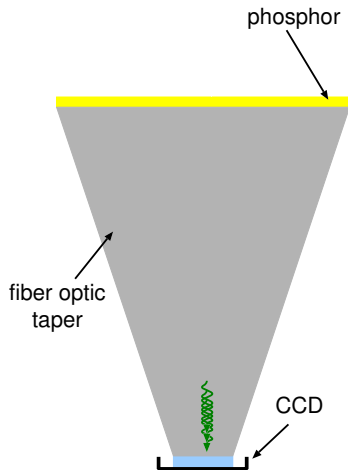
The largest area detectors are made using the CCD in indirect mode

The CCD is coupled optically to a fiber optic taper which ends at a large phosphor

When an x-ray is absorbed at the phosphor, visible light photons are emitted in all directions

A fraction of the visible light is guided to the CCD chip(s) at the end of the taper

This detector requires careful geometric corrections, particularly with multiple CCD arrays



## CCD detectors - indirect

The largest area detectors are made using the CCD in indirect mode

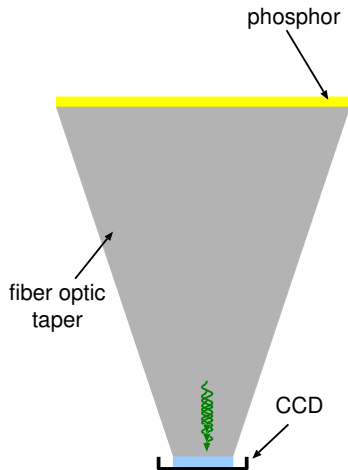
The CCD is coupled optically to a fiber optic taper which ends at a large phosphor

When an x-ray is absorbed at the phosphor, visible light photons are emitted in all directions

A fraction of the visible light is guided to the CCD chip(s) at the end of the taper

This detector requires careful geometric corrections, particularly with multiple CCD arrays

Pixel sizes are usually rather large ( $50 \mu\text{m} \times 50 \mu\text{m}$ )

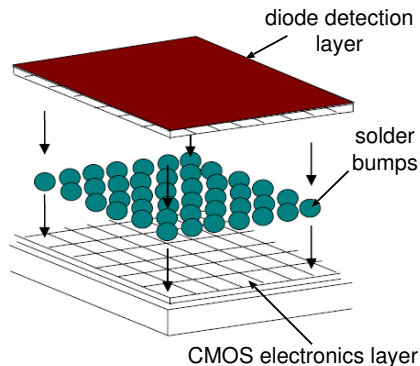




## Pixel array detectors - schematic

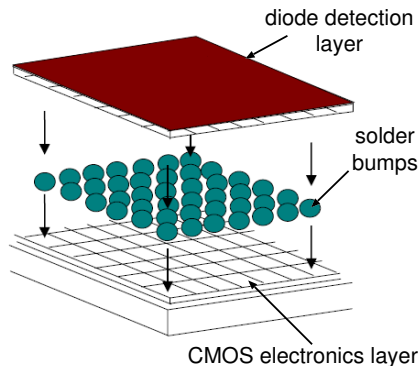
The Pixel Array Detector combines area detection with on-board electronics for fast signal processing

## Pixel array detectors - schematic



The Pixel Array Detector combines area detection with on-board electronics for fast signal processing

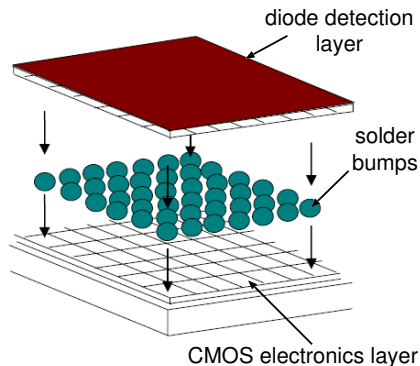
## Pixel array detectors - schematic



The Pixel Array Detector combines area detection with on-board electronics for fast signal processing

The diode layer absorbs x-rays and the electron-hole pairs are immediately swept into the CMOS electronics layer

## Pixel array detectors - schematic

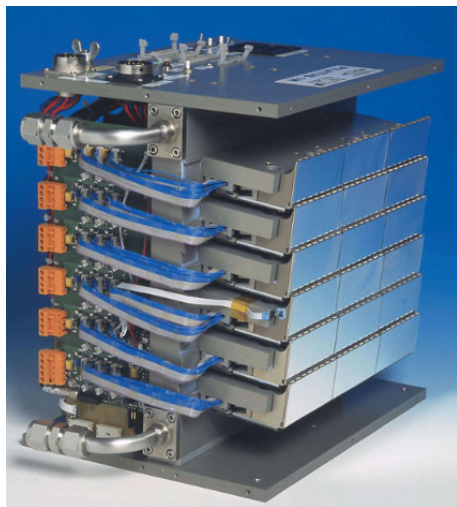


The Pixel Array Detector combines area detection with on-board electronics for fast signal processing

The diode layer absorbs x-rays and the electron-hole pairs are immediately swept into the CMOS electronics layer

This permits fast processing and possibly energy discrimination on a per-pixel level

## Pixel array detectors - Pilatus



Pixel array detector with 1,000,000 pixels.

Each pixel has energy resolving capabilities & high speed readout.

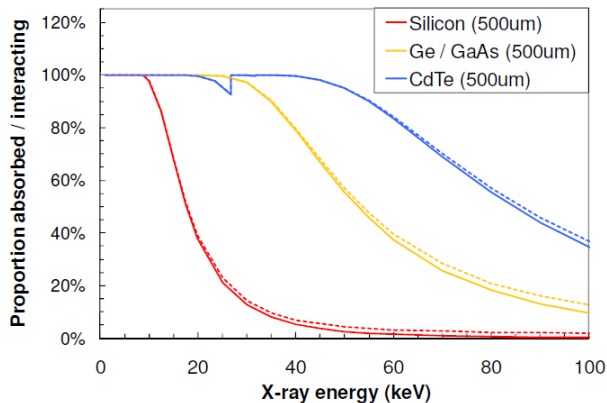
Silicon sensor limits energy range of operation.

from Swiss Light Source

# High energy solutions

One of the major problems with pixel array detectors and SDDs is the low absorption cross section at high energies

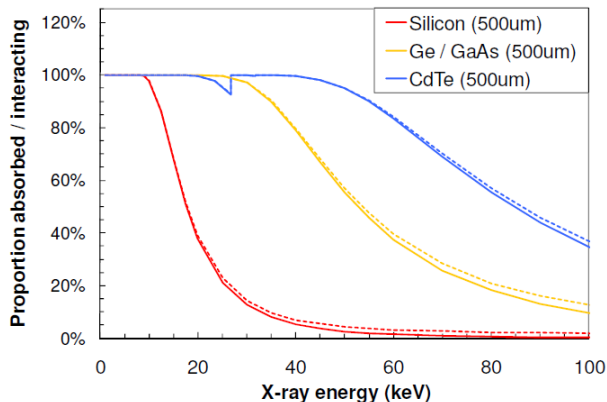
# High energy solutions



One of the major problems with pixel array detectors and SDDs is the low absorption cross section at high energies

One solution is to use a semiconductor other than Si, for example Ge, GaAs or, CdTe

## High energy solutions



One of the major problems with pixel array detectors and SDDs is the low absorption cross section at high energies

One solution is to use a semiconductor other than Si, for example Ge, GaAs or, CdTe

The absorption can be significantly enhanced with these higher Z elements while maintaining good energy discrimination capabilities.



## Refractive index in the x-ray region

When visible light passes from one medium to another, it changes direction according to Snell's Law which depends on the index of refraction of the two media.

## Refractive index in the x-ray region

When visible light passes from one medium to another, it changes direction according to Snell's Law which depends on the index of refraction of the two media.

For visible light, the index of refraction of a transparent medium is always greater than unity and this is exploited to create lenses and optical devices.

## Refractive index in the x-ray region

When visible light passes from one medium to another, it changes direction according to Snell's Law which depends on the index of refraction of the two media.

For visible light, the index of refraction of a transparent medium is always greater than unity and this is exploited to create lenses and optical devices.

For x-rays, there is also an index of refraction but it is always slightly less than unity, resulting in phenomena which can be used to create x-ray optics and a host of experimental techniques.

## Refractive index in the x-ray region

When visible light passes from one medium to another, it changes direction according to Snell's Law which depends on the index of refraction of the two media.

For visible light, the index of refraction of a transparent medium is always greater than unity and this is exploited to create lenses and optical devices.

For x-rays, there is also an index of refraction but it is always slightly less than unity, resulting in phenomena which can be used to create x-ray optics and a host of experimental techniques.

The refraction and reflection of x-rays derive fundamentally from the scattering of x-rays by electrons and the fact that the scattering factor is negative,  $-r_0$ .

## Refractive index in the x-ray region

When visible light passes from one medium to another, it changes direction according to Snell's Law which depends on the index of refraction of the two media.

For visible light, the index of refraction of a transparent medium is always greater than unity and this is exploited to create lenses and optical devices.

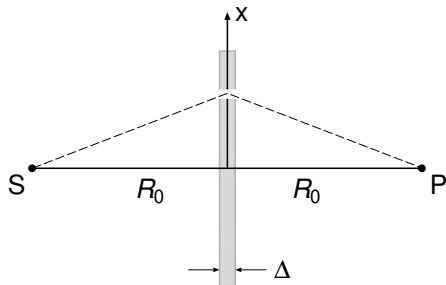
For x-rays, there is also an index of refraction but it is always slightly less than unity, resulting in phenomena which can be used to create x-ray optics and a host of experimental techniques.

The refraction and reflection of x-rays derive fundamentally from the scattering of x-rays by electrons and the fact that the scattering factor is negative,  $-r_0$ .

Initially assume that all interfaces are perfectly flat and ignore all absorption processes.

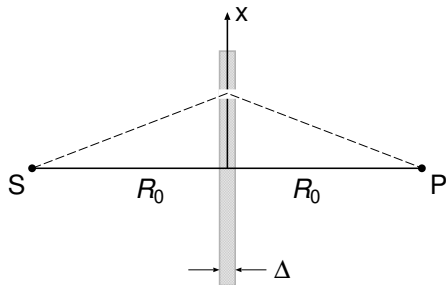
## Thin plate response - scattering approach

Consider a thin plate of thickness  $\Delta$  onto which x-rays are incident from a point source  $S$  a perpendicular distance  $R_0$  away.



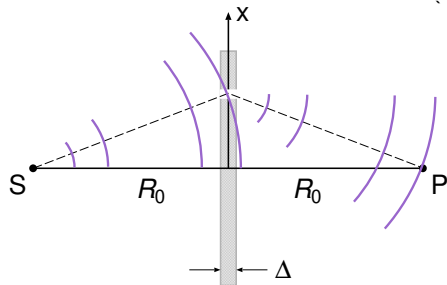
## Thin plate response - scattering approach

Consider a thin plate of thickness  $\Delta$  onto which x-rays are incident from a point source  $S$  a perpendicular distance  $R_0$  away. A detector is placed at  $P$ , also a perpendicular distance  $R_0$  on the other side of the plate.



## Thin plate response - scattering approach

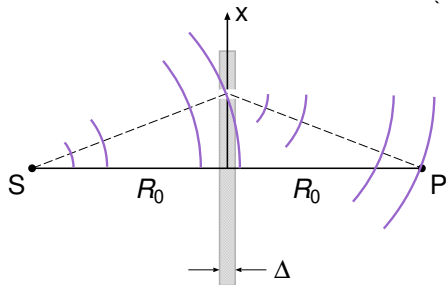
Consider a thin plate of thickness  $\Delta$  onto which x-rays are incident from a point source  $S$  a perpendicular distance  $R_0$  away. A detector is placed at  $P$ , also a perpendicular distance  $R_0$  on the other side of the plate. We consider a small volume at location  $(x, y)$  which scatters the x-rays.





## Thin plate response - scattering approach

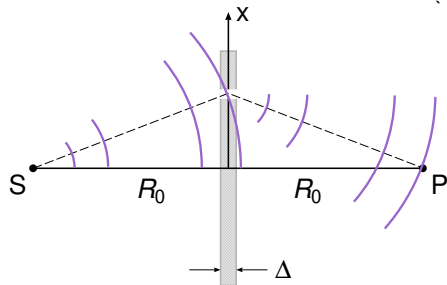
Consider a thin plate of thickness  $\Delta$  onto which x-rays are incident from a point source  $S$  a perpendicular distance  $R_0$  away. A detector is placed at  $P$ , also a perpendicular distance  $R_0$  on the other side of the plate. We consider a small volume at location  $(x, y)$  which scatters the x-rays.



The plate has electron density  $\rho$  and the volume  $\Delta dx dy$  contains  $\rho \Delta dx dy$  electrons which scatter the x-rays.

## Thin plate response - scattering approach

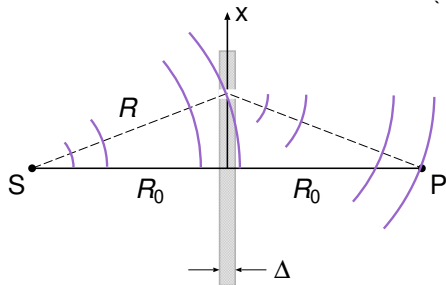
Consider a thin plate of thickness  $\Delta$  onto which x-rays are incident from a point source  $S$  a perpendicular distance  $R_0$  away. A detector is placed at  $P$ , also a perpendicular distance  $R_0$  on the other side of the plate. We consider a small volume at location  $(x, y)$  which scatters the x-rays.



The plate has electron density  $\rho$  and the volume  $\Delta dx dy$  contains  $\rho \Delta dx dy$  electrons which scatter the x-rays. The distance from  $S$  to the scattering volume is

## Thin plate response - scattering approach

Consider a thin plate of thickness  $\Delta$  onto which x-rays are incident from a point source  $S$  a perpendicular distance  $R_0$  away. A detector is placed at  $P$ , also a perpendicular distance  $R_0$  on the other side of the plate. We consider a small volume at location  $(x, y)$  which scatters the x-rays.

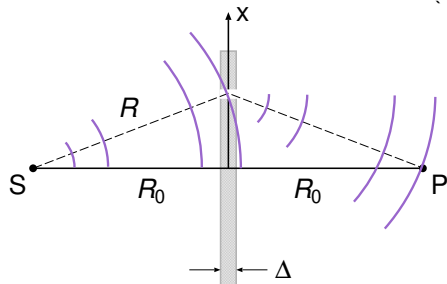


The plate has electron density  $\rho$  and the volume  $\Delta dx dy$  contains  $\rho \Delta dx dy$  electrons which scatter the x-rays. The distance from  $S$  to the scattering volume is

$$R = \sqrt{R_0^2 + x^2 + y^2}$$

## Thin plate response - scattering approach

Consider a thin plate of thickness  $\Delta$  onto which x-rays are incident from a point source  $S$  a perpendicular distance  $R_0$  away. A detector is placed at  $P$ , also a perpendicular distance  $R_0$  on the other side of the plate. We consider a small volume at location  $(x, y)$  which scatters the x-rays.



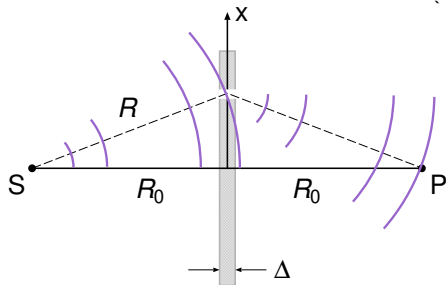
The plate has electron density  $\rho$  and the volume  $\Delta dx dy$  contains  $\rho \Delta dx dy$  electrons which scatter the x-rays. The distance from  $S$  to the scattering volume is

$$R = \sqrt{R_0^2 + x^2 + y^2}$$

$$R = R_0 \sqrt{1 + \frac{x^2 + y^2}{R_0^2}}$$

## Thin plate response - scattering approach

Consider a thin plate of thickness  $\Delta$  onto which x-rays are incident from a point source  $S$  a perpendicular distance  $R_0$  away. A detector is placed at  $P$ , also a perpendicular distance  $R_0$  on the other side of the plate. We consider a small volume at location  $(x, y)$  which scatters the x-rays.



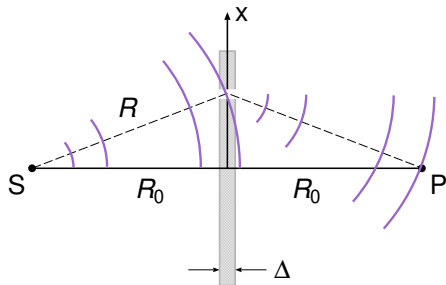
The plate has electron density  $\rho$  and the volume  $\Delta dx dy$  contains  $\rho \Delta dx dy$  electrons which scatter the x-rays. The distance from  $S$  to the scattering volume is

$$R = \sqrt{R_0^2 + x^2 + y^2}$$

$$R = R_0 \sqrt{1 + \frac{x^2 + y^2}{R_0^2}} \approx R_0 \left[ 1 + \frac{x^2 + y^2}{2R_0^2} \right]$$

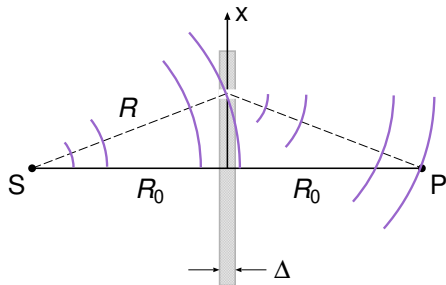
## Thin plate response - scattering approach

$R$  is also the distance between the scattering volume and  $P$  so, a wave (x-ray) which travels from  $S \rightarrow P$  through the scattering volume will have an extra phase shift



## Thin plate response - scattering approach

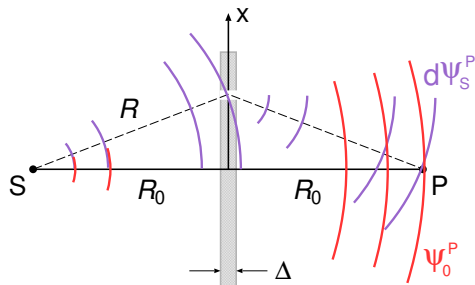
$R$  is also the distance between the scattering volume and  $P$  so, a wave (x-ray) which travels from  $S \rightarrow P$  through the scattering volume will have an extra phase shift



$$\phi(x, y) = 2k \frac{x^2 + y^2}{2R_0^2}$$

## Thin plate response - scattering approach

$R$  is also the distance between the scattering volume and  $P$  so, a wave (x-ray) which travels from  $S \rightarrow P$  through the scattering volume will have an extra phase shift



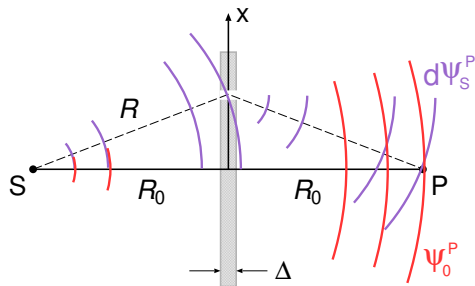
$$\phi(x, y) = 2k \frac{x^2 + y^2}{2R_0^2} = \frac{x^2 + y^2}{R_0^2} k$$

compared to a wave which travels directly along the  $z$ -axis.



## Thin plate response - scattering approach

$R$  is also the distance between the scattering volume and  $P$  so, a wave (x-ray) which travels from  $S \rightarrow P$  through the scattering volume will have an extra phase shift

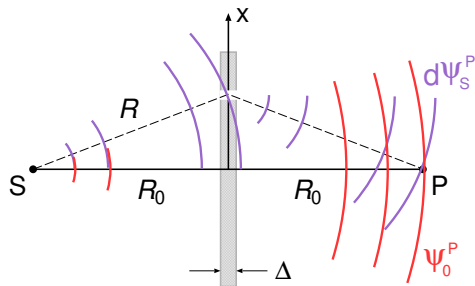


$$\phi(x, y) = 2k \frac{x^2 + y^2}{2R_0^2} = \frac{x^2 + y^2}{R_0^2} k$$

compared to a wave which travels directly along the  $z$ -axis. The wave which is scattered through the volume will have the form

## Thin plate response - scattering approach

$R$  is also the distance between the scattering volume and  $P$  so, a wave (x-ray) which travels from  $S \rightarrow P$  through the scattering volume will have an extra phase shift



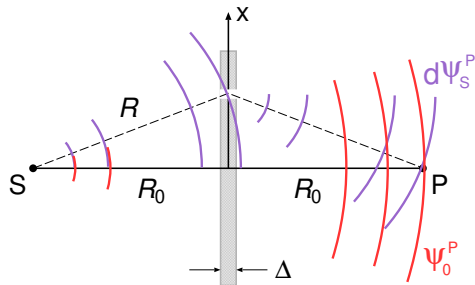
$$\phi(x, y) = 2k \frac{x^2 + y^2}{2R_0^2} = \frac{x^2 + y^2}{R_0^2} k$$

compared to a wave which travels directly along the  $z$ -axis. The wave which is scattered through the volume will have the form

$$d\psi_S^P \approx \left( \frac{e^{ikR_0}}{R_0} \right)$$

## Thin plate response - scattering approach

$R$  is also the distance between the scattering volume and  $P$  so, a wave (x-ray) which travels from  $S \rightarrow P$  through the scattering volume will have an extra phase shift



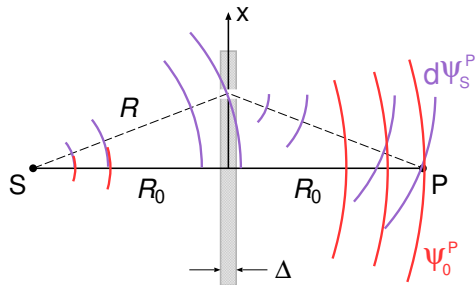
$$\phi(x, y) = 2k \frac{x^2 + y^2}{2R_0^2} = \frac{x^2 + y^2}{R_0^2} k$$

compared to a wave which travels directly along the  $z$ -axis. The wave which is scattered through the volume will have the form

$$d\psi_S^P \approx \left( \frac{e^{ikR_0}}{R_0} \right) (\rho \Delta dx dy)$$

## Thin plate response - scattering approach

$R$  is also the distance between the scattering volume and  $P$  so, a wave (x-ray) which travels from  $S \rightarrow P$  through the scattering volume will have an extra phase shift



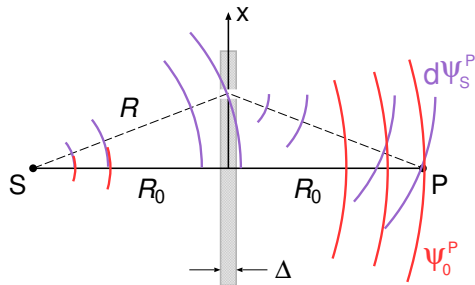
$$\phi(x, y) = 2k \frac{x^2 + y^2}{2R_0^2} = \frac{x^2 + y^2}{R_0^2} k$$

compared to a wave which travels directly along the  $z$ -axis. The wave which is scattered through the volume will have the form

$$d\psi_S^P \approx \left( \frac{e^{ikR_0}}{R_0} \right) (\rho \Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right)$$

## Thin plate response - scattering approach

$R$  is also the distance between the scattering volume and  $P$  so, a wave (x-ray) which travels from  $S \rightarrow P$  through the scattering volume will have an extra phase shift



$$\phi(x, y) = 2k \frac{x^2 + y^2}{2R_0^2} = \frac{x^2 + y^2}{R_0^2} k$$

compared to a wave which travels directly along the  $z$ -axis. The wave which is scattered through the volume will have the form

$$d\psi_S^P \approx \left( \frac{e^{ikR_0}}{R_0} \right) (\rho \Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x, y)}$$

## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

Integrate the scattered wave over the entire plate.

## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

$$\psi_S^P = \int d\psi_S^P = -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy$$

Integrate the scattered wave over the entire plate. This integral is basically a Gaussian integral squared with an imaginary (instead of real) constant in the exponent and it gives



## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dxdy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

$$\psi_S^P = \int d\psi_S^P = -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dxdy$$

Integrate the scattered wave over the entire plate. This integral is basically a Gaussian integral squared with an imaginary (instead of real) constant in the exponent and it gives

$$\int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dxdy = i \frac{\pi R_0^2}{k}$$

## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

$$\begin{aligned} \psi_S^P &= \int d\psi_S^P = -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy \\ &= -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \left( i \frac{\pi R_0}{k} \right) \end{aligned}$$

Integrate the scattered wave over the entire plate. This integral is basically a Gaussian integral squared with an imaginary (instead of real) constant in the exponent and it gives

$$\int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy = i \frac{\pi R_0}{k}$$

## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dxdy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

$$\begin{aligned} \psi_S^P &= \int d\psi_S^P = -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dxdy \\ &= -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \left( i \frac{\pi R_0}{k} \right) \end{aligned}$$

Integrate the scattered wave over the entire plate. This integral is basically a Gaussian integral squared with an imaginary (instead of real) constant in the exponent and it gives

$$\int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dxdy = i \frac{\pi R_0}{k}$$

Thus the total wave (electric field) at  $P$  can be written

## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

$$\begin{aligned} \psi_S^P &= \int d\psi_S^P = -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy \\ &= -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \left( i \frac{\pi R_0}{k} \right) \end{aligned}$$

$$\psi^P = \psi_0^P + \psi_S^P$$

Integrate the scattered wave over the entire plate. This integral is basically a Gaussian integral squared with an imaginary (instead of real) constant in the exponent and it gives

$$\int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy = i \frac{\pi R_0}{k}$$

Thus the total wave (electric field) at  $P$  can be written

## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

$$\begin{aligned} \psi_S^P &= \int d\psi_S^P = -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy \\ &= -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \left( i \frac{\pi R_0}{k} \right) \end{aligned}$$

$$\begin{aligned} \psi^P &= \psi_0^P + \psi_S^P \\ &= \frac{e^{i2kR_0}}{2R_0} - i \rho b \Delta \frac{\pi R_0}{k} \frac{e^{i2kR_0}}{R_0^2} \end{aligned}$$

Integrate the scattered wave over the entire plate. This integral is basically a Gaussian integral squared with an imaginary (instead of real) constant in the exponent and it gives

$$\int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy = i \frac{\pi R_0}{k}$$

Thus the total wave (electric field) at  $P$  can be written

## Thin plate response - scattering approach

$$d\psi_S^P = \left( \frac{e^{ikR_0}}{R_0} \right) \rho(\Delta dx dy) \left( -b \frac{e^{ikR_0}}{R_0} \right) e^{i\phi(x,y)}$$

$$\begin{aligned} \psi_S^P &= \int d\psi_S^P = -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy \\ &= -\rho b \Delta \frac{e^{i2kR_0}}{R_0^2} \left( i \frac{\pi R_0}{k} \right) \end{aligned}$$

$$\begin{aligned} \psi^P &= \psi_0^P + \psi_S^P \\ &= \frac{e^{i2kR_0}}{2R_0} - i \rho b \Delta \frac{\pi R_0}{k} \frac{e^{i2kR_0}}{R_0^2} \\ &= \psi_0^P \left[ 1 - i \frac{2\pi \rho b \Delta}{k} \right] \end{aligned}$$

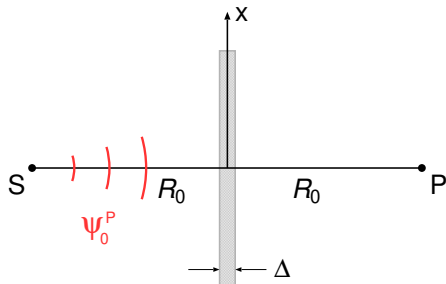
Integrate the scattered wave over the entire plate. This integral is basically a Gaussian integral squared with an imaginary (instead of real) constant in the exponent and it gives

$$\int_{-\infty}^{\infty} e^{i \frac{x^2+y^2}{R_0^2} k} dx dy = i \frac{\pi R_0}{k}$$

Thus the total wave (electric field) at  $P$  can be written

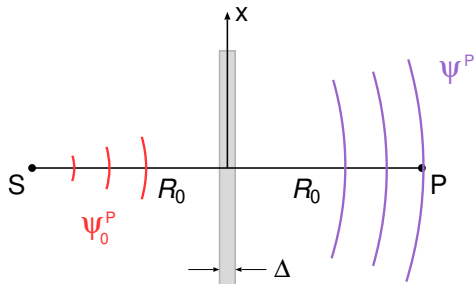
## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction.



## Thin plate response - refraction approach

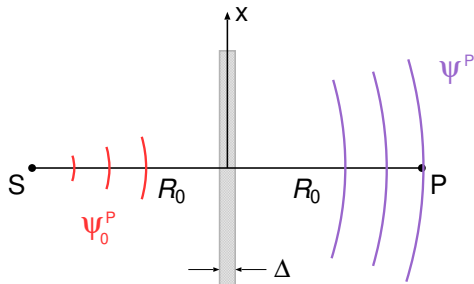
Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.





## Thin plate response - refraction approach

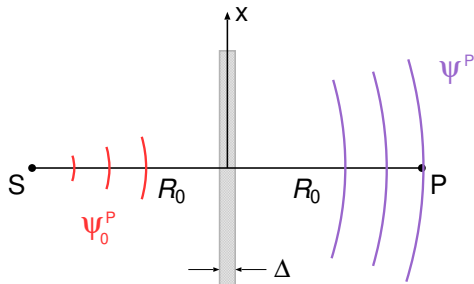
Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.



The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.

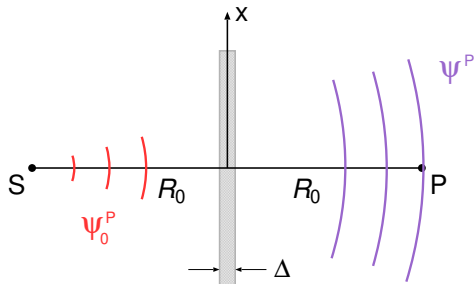


The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

$$\phi = 2\pi \left( \frac{\Delta}{\lambda'} - \frac{\Delta}{\lambda} \right)$$

## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.

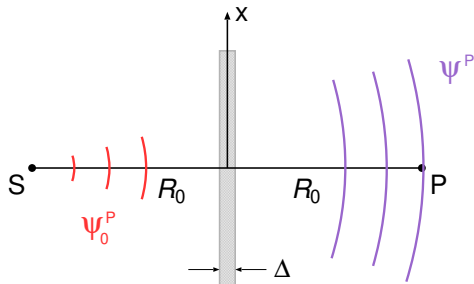


The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

$$\phi = 2\pi \left( \frac{n\Delta}{\lambda} - \frac{\Delta}{\lambda} \right)$$

## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.

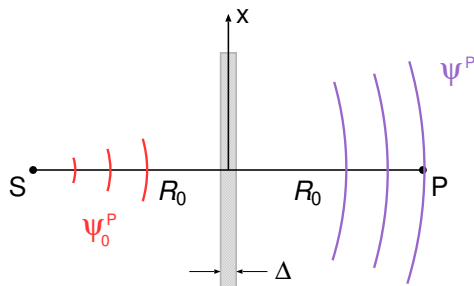


The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

$$\begin{aligned}\phi &= 2\pi \left( \frac{n\Delta}{\lambda} - \frac{\Delta}{\lambda} \right) \\ &= \frac{2\pi}{\lambda} \Delta (n - 1)\end{aligned}$$

## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.

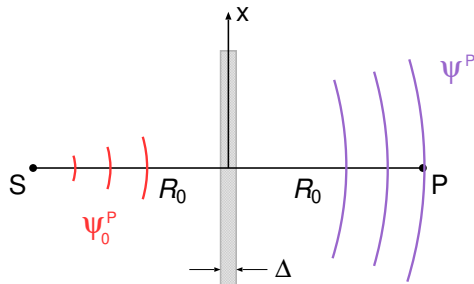


The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

$$\begin{aligned}\phi &= 2\pi \left( \frac{n\Delta}{\lambda} - \frac{\Delta}{\lambda} \right) \\ &= \frac{2\pi}{\lambda} \Delta (n - 1) = k\Delta (n - 1)\end{aligned}$$

## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.



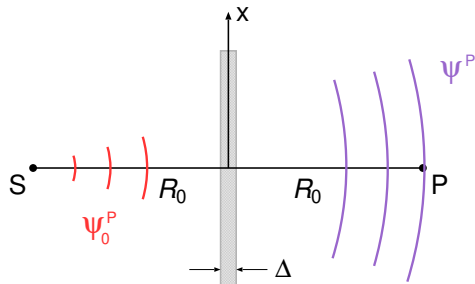
The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

$$\begin{aligned}\phi &= 2\pi \left( \frac{n\Delta}{\lambda} - \frac{\Delta}{\lambda} \right) \\ &= \frac{2\pi}{\lambda} \Delta (n - 1) = k\Delta (n - 1)\end{aligned}$$

The wave function at  $P$  is then:

## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.



The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

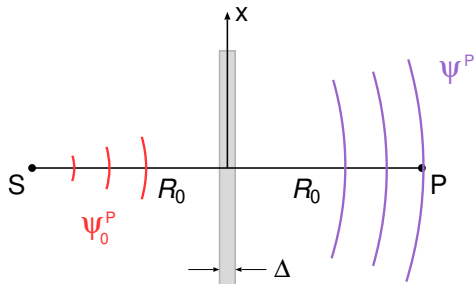
$$\begin{aligned}\phi &= 2\pi \left( \frac{n\Delta}{\lambda} - \frac{\Delta}{\lambda} \right) \\ &= \frac{2\pi}{\lambda} \Delta (n - 1) = k\Delta (n - 1)\end{aligned}$$

The wave function at  $P$  is then:

$$\psi^P = \psi_0^P e^{i(n-1)k\Delta}$$

## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.



The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

$$\begin{aligned}\phi &= 2\pi \left( \frac{n\Delta}{\lambda} - \frac{\Delta}{\lambda} \right) \\ &= \frac{2\pi}{\lambda} \Delta (n - 1) = k\Delta (n - 1)\end{aligned}$$

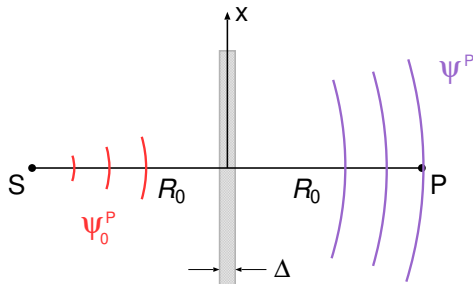
The wave function at  $P$  is then:

$$\psi^P = \psi_0^P e^{i(n-1)k\Delta} = \psi_0^P [1 + i(n-1)k\Delta + \dots]$$



## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction. Assume that the wave passing through the plate simply gains a phase shift because it passes through a medium compared to a wave which does not have the plate present.



The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

$$\begin{aligned}\phi &= 2\pi \left( \frac{n\Delta}{\lambda} - \frac{\Delta}{\lambda} \right) \\ &= \frac{2\pi}{\lambda} \Delta (n - 1) = k\Delta (n - 1)\end{aligned}$$

The wave function at  $P$  is then:

$$\psi^P = \psi_0^P e^{i(n-1)k\Delta} = \psi_0^P [1 + i(n-1)k\Delta + \dots] \approx \psi_0^P [1 + i(n-1)k\Delta]$$

## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

Scattering

Refraction

## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

Scattering

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$

Refraction

$$\psi^P = \psi_0^P [1 + i(n - 1)k\Delta]$$

## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

Scattering

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$

Refraction

$$\psi^P = \psi_0^P [1 + i(n - 1)k\Delta]$$

By inspection we have

## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

Scattering

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$

Refraction

$$\psi^P = \psi_0^P [1 + i(n - 1)k\Delta]$$

By inspection we have

$$(n - 1)k\Delta = -\frac{2\pi\rho b\Delta}{k}$$

## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

Scattering

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$

Refraction

$$\psi^P = \psi_0^P [1 + i(n - 1)k\Delta]$$

By inspection we have

$$\begin{aligned}(n - 1)k\Delta &= -\frac{2\pi\rho b\Delta}{k} \\ n - 1 &= -\frac{2\pi\rho b}{k^2}\end{aligned}$$

## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

Scattering

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$

Refraction

$$\psi^P = \psi_0^P [1 + i(n - 1)k\Delta]$$

By inspection we have

$$(n - 1)k\Delta = -\frac{2\pi\rho b\Delta}{k}$$

$$n - 1 = -\frac{2\pi\rho b}{k^2}$$

$$n = 1 - \frac{2\pi\rho b}{k^2}$$



## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

Scattering

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$

Refraction

$$\psi^P = \psi_0^P [1 + i(n - 1)k\Delta]$$

By inspection we have

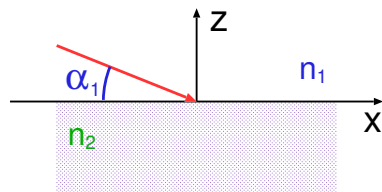
$$(n - 1)k\Delta = -\frac{2\pi\rho b\Delta}{k}$$

$$n - 1 = -\frac{2\pi\rho b}{k^2}$$

$$n = 1 - \frac{2\pi\rho b}{k^2} = 1 - \delta$$

## Index of refraction & critical angle

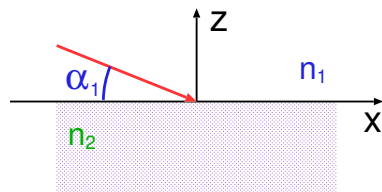
Now that we have an expression for the index of refraction, we can examine the consequences and estimate it's magnitude.



## Index of refraction & critical angle

Now that we have an expression for the index of refraction, we can examine the consequences and estimate it's magnitude.

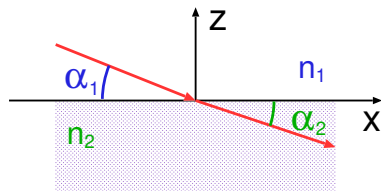
Consider an x-ray incident on an interface at angle  $\alpha_1$  to the surface



## Index of refraction & critical angle

Now that we have an expression for the index of refraction, we can examine the consequences and estimate its magnitude.

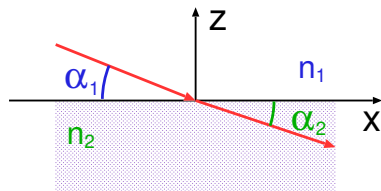
Consider an x-ray incident on an interface at angle  $\alpha_1$  to the surface which is refracted into the medium of index  $n_2$  at angle  $\alpha_2$ .



## Index of refraction & critical angle

Now that we have an expression for the index of refraction, we can examine the consequences and estimate its magnitude.

Consider an x-ray incident on an interface at angle  $\alpha_1$  to the surface which is refracted into the medium of index  $n_2$  at angle  $\alpha_2$ .



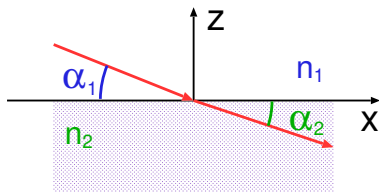
Applying Snell's Law

$$n_1 \cos \alpha_1 = n_2 \cos \alpha_2$$

## Index of refraction & critical angle

Now that we have an expression for the index of refraction, we can examine the consequences and estimate its magnitude.

Consider an x-ray incident on an interface at angle  $\alpha_1$  to the surface which is refracted into the medium of index  $n_2$  at angle  $\alpha_2$ .



Applying Snell's Law, and assuming that the incident medium is air (vacuum).

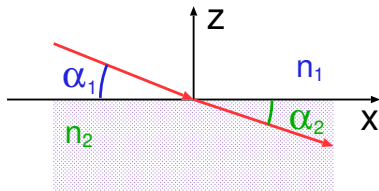
$$n_1 \cos \alpha_1 = n_2 \cos \alpha_2$$

$$\cos \alpha_1 = n_2 \cos \alpha_2$$

## Index of refraction & critical angle

Now that we have an expression for the index of refraction, we can examine the consequences and estimate its magnitude.

Consider an x-ray incident on an interface at angle  $\alpha_1$  to the surface which is refracted into the medium of index  $n_2$  at angle  $\alpha_2$ .



Applying Snell's Law, and assuming that the incident medium is air (vacuum).

If we now apply the known form of the index of refraction for the medium ( $n_2 = 1 - \delta$ ).

$$n_1 \cos \alpha_1 = n_2 \cos \alpha_2$$

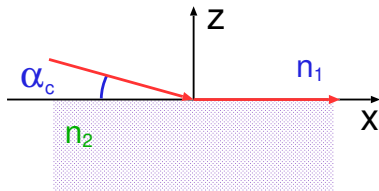
$$\cos \alpha_1 = n_2 \cos \alpha_2$$

$$\cos \alpha_1 = (1 - \delta) \cos \alpha_2$$

## Index of refraction & critical angle

Now that we have an expression for the index of refraction, we can examine the consequences and estimate its magnitude.

Consider an x-ray incident on an interface at angle  $\alpha_1$  to the surface which is refracted into the medium of index  $n_2$  at angle  $\alpha_2$ .



Applying Snell's Law, and assuming that the incident medium is air (vacuum).

If we now apply the known form of the index of refraction for the medium ( $n_2 = 1 - \delta$ ).

When the incident angle becomes small enough, there will be total external reflection

$$n_1 \cos \alpha_1 = n_2 \cos \alpha_2$$

$$\cos \alpha_1 = n_2 \cos \alpha_2$$

$$\cos \alpha_1 = (1 - \delta) \cos \alpha_2$$

$$\cos \alpha_c = 1 - \delta$$



# Estimation of critical angle

$$1 - \delta = \cos \alpha_c$$

# Estimation of critical angle

For small angles, the cosine function can be expanded

$$1 - \delta = \cos \alpha_c$$

$$1 - \delta = 1 - \frac{\alpha_c^2}{2} + \dots$$

# Estimation of critical angle

For small angles, the cosine function can be expanded

$$1 - \delta = \cos \alpha_c$$

$$1 - \delta = 1 - \frac{\alpha_c^2}{2} + \dots$$

$$1 - \delta \approx 1 - \frac{\alpha_c^2}{2}$$

## Estimation of critical angle

For small angles, the cosine function can be expanded to give a simple relation for the critical angle

$$1 - \delta = \cos \alpha_c$$

$$1 - \delta = 1 - \frac{\alpha_c^2}{2} + \dots$$

$$1 - \delta \approx 1 - \frac{\alpha_c^2}{2}$$

$$\delta \approx \frac{\alpha_c^2}{2}$$

$$\alpha_c = \sqrt{2\delta}$$

# Estimation of critical angle

For small angles, the cosine function can be expanded to give a simple relation for the critical angle

If  $\delta \sim 10^{-5}$ , then the critical angle is

$$1 - \delta = \cos \alpha_c$$

$$1 - \delta = 1 - \frac{\alpha_c^2}{2} + \dots$$

$$1 - \delta \approx 1 - \frac{\alpha_c^2}{2}$$

$$\delta \approx \frac{\alpha_c^2}{2}$$

$$\alpha_c = \sqrt{2\delta}$$

$$\alpha_c = \sqrt{2 \times 10^{-5}}$$

# Estimation of critical angle

For small angles, the cosine function can be expanded to give a simple relation for the critical angle

If  $\delta \sim 10^{-5}$ , then the critical angle is

$$1 - \delta = \cos \alpha_c$$

$$1 - \delta = 1 - \frac{\alpha_c^2}{2} + \dots$$

$$1 - \delta \approx 1 - \frac{\alpha_c^2}{2}$$

$$\delta \approx \frac{\alpha_c^2}{2}$$

$$\alpha_c = \sqrt{2\delta}$$

$$\begin{aligned}\alpha_c &= \sqrt{2 \times 10^{-5}} \\ &= 4.5 \times 10^{-3} = 4.5 \text{ mrad}\end{aligned}$$

## Estimation of critical angle

For small angles, the cosine function can be expanded to give a simple relation for the critical angle

If  $\delta \sim 10^{-5}$ , then the critical angle is

$$1 - \delta = \cos \alpha_c$$

$$1 - \delta = 1 - \frac{\alpha_c^2}{2} + \dots$$

$$1 - \delta \approx 1 - \frac{\alpha_c^2}{2}$$

$$\delta \approx \frac{\alpha_c^2}{2}$$

$$\alpha_c = \sqrt{2\delta}$$

$$\begin{aligned}\alpha_c &= \sqrt{2 \times 10^{-5}} \\ &= 4.5 \times 10^{-3} = 4.5 \text{ mrad} \\ &= 0.26^\circ\end{aligned}$$

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$



## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

Therefore, it is useful to replace the uniform charge distribution,  $\rho$ , with a more realistic one, including the atom distribution  $\rho_a$ :

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

Therefore, it is useful to replace the uniform charge distribution,  $\rho$ , with a more realistic one, including the atom distribution  $\rho_a$ :

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$

$$\rho = \rho_a f^0(\theta = 90^\circ)$$

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

Therefore, it is useful to replace the uniform charge distribution,  $\rho$ , with a more realistic one, including the atom distribution  $\rho_a$ :

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi\rho b\Delta}{k} \right]$$
$$\rho = \rho_a f^0(\theta = 90^\circ)$$

This holds for forward scattering ( $\theta = 90^\circ$  or  $\psi = 0^\circ$ ) only, and a correction term of  $\sin \theta$  is needed if the viewing angle is different.

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

Therefore, it is useful to replace the uniform charge distribution,  $\rho$ , with a more realistic one, including the atom distribution  $\rho_a$ :

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi \rho b \Delta}{k} \right]$$
$$\rho = \rho_a f^0(\theta = 90^\circ) \quad k = 2\pi/\lambda$$

This holds for forward scattering ( $\theta = 90^\circ$  or  $\psi = 0^\circ$ ) only, and a correction term of  $\sin \theta$  is needed if the viewing angle is different.

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

Therefore, it is useful to replace the uniform charge distribution,  $\rho$ , with a more realistic one, including the atom distribution  $\rho_a$ :

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi \rho b \Delta}{k} \right]$$
$$\rho = \rho_a f^0(\theta = 90^\circ) \quad k = 2\pi/\lambda$$

This holds for forward scattering ( $\theta = 90^\circ$  or  $\psi = 0^\circ$ ) only, and a correction term of  $\sin \theta$  is needed if the viewing angle is different.

$$\psi^P = \psi_0^P \left[ 1 - i \frac{\lambda \rho_a f^0 r_0 \Delta}{\sin \theta} \right]$$

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

Therefore, it is useful to replace the uniform charge distribution,  $\rho$ , with a more realistic one, including the atom distribution  $\rho_a$ :

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi \rho b \Delta}{k} \right]$$
$$\rho = \rho_a f^0(\theta = 90^\circ) \quad k = 2\pi/\lambda$$

This holds for forward scattering ( $\theta = 90^\circ$  or  $\psi = 0^\circ$ ) only, and a correction term of  $\sin \theta$  is needed if the viewing angle is different.

$$\psi^P = \psi_0^P \left[ 1 - i \frac{\lambda \rho_a f^0 r_0 \Delta}{\sin \theta} \right]$$

$$\psi^P = \psi_0^P [1 - ig_0]$$

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

Therefore, it is useful to replace the uniform charge distribution,  $\rho$ , with a more realistic one, including the atom distribution  $\rho_a$ :

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi \rho b \Delta}{k} \right]$$
$$\rho = \rho_a f^0(\theta = 90^\circ) \quad k = 2\pi/\lambda$$

$$\psi^P = \psi_0^P \left[ 1 - i \frac{\lambda \rho_a f^0 r_0 \Delta}{\sin \theta} \right]$$

$$\psi^P = \psi_0^P [1 - ig_0]$$

This holds for forward scattering ( $\theta = 90^\circ$  or  $\psi = 0^\circ$ ) only, and a correction term of  $\sin \theta$  is needed if the viewing angle is different.

The second term is the first order term in the expansion of a complex exponential and thus is nothing more than a phase shift to the electromagnetic wave.

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.

Therefore, it is useful to replace the uniform charge distribution,  $\rho$ , with a more realistic one, including the atom distribution  $\rho_a$ :

$$\psi^P = \psi_0^P \left[ 1 - i \frac{2\pi \rho b \Delta}{k} \right]$$
$$\rho = \rho_a f^0(\theta = 90^\circ) \quad k = 2\pi/\lambda$$

$$\psi^P = \psi_0^P \left[ 1 - i \frac{\lambda \rho_a f^0 r_0 \Delta}{\sin \theta} \right]$$

$$\psi^P = \psi_0^P [1 - ig_0] \approx \psi_0^P e^{-ig_0}$$

This holds for forward scattering ( $\theta = 90^\circ$  or  $\psi = 0^\circ$ ) only, and a correction term of  $\sin \theta$  is needed if the viewing angle is different.

The second term is the first order term in the expansion of a complex exponential and thus is nothing more than a phase shift to the electromagnetic wave.



## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

$$n = 1 - \delta + i\beta$$

## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

Begin with Beer's Law for absorption

$$n = 1 - \delta + i\beta$$

## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

Begin with Beer's Law for absorption

$$n = 1 - \delta + i\beta$$

$$I(z) = I_0 e^{-\mu z}$$

## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

Begin with Beer’s Law for absorption

$$n = 1 - \delta + i\beta$$

In the refractive approach, the wave propagating in the medium is modified by the index of refraction  $k' = nk$  so that

$$I(z) = I_0 e^{-\mu z}$$

## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

Begin with Beer’s Law for absorption

$$n = 1 - \delta + i\beta$$

In the refractive approach, the wave propagating in the medium is modified by the index of refraction  $k' = nk$  so that

$$I(z) = I_0 e^{-\mu z}$$

$$e^{inkz} = e^{i(1-\delta+i\beta)kz}$$

## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

Begin with Beer’s Law for absorption

$$n = 1 - \delta + i\beta$$

In the refractive approach, the wave propagating in the medium is modified by the index of refraction  $k' = nk$  so that

$$I(z) = I_0 e^{-\mu z}$$

$$\begin{aligned} e^{inkz} &= e^{i(1-\delta+i\beta)kz} \\ &= e^{i(1-\delta)kz} e^{-\beta kz} \end{aligned}$$

## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

Begin with Beer’s Law for absorption

$$n = 1 - \delta + i\beta$$

In the refractive approach, the wave propagating in the medium is modified by the index of refraction  $k' = nk$  so that

$$I(z) = I_0 e^{-\mu z}$$

$$\begin{aligned} e^{inkz} &= e^{i(1-\delta+i\beta)kz} \\ &= e^{i(1-\delta)kz} e^{-\beta kz} \end{aligned}$$

The real exponential can be compared with Beer’s Law, noting that intensity is proportional to the **square** of the wave function



## Absorption term in $n$

Since the actual scattering factor of an atom has resonant (“anomalous”) terms,  $f(Q) = f^0(Q) + f' + if''$ , we must include an absorption term in the model for the index of refraction.

Begin with Beer’s Law for absorption

$$n = 1 - \delta + i\beta$$

In the refractive approach, the wave propagating in the medium is modified by the index of refraction  $k' = nk$  so that

$$I(z) = I_0 e^{-\mu z}$$

$$\begin{aligned} e^{inkz} &= e^{i(1-\delta+i\beta)kz} \\ &= e^{i(1-\delta)kz} e^{-\beta kz} \end{aligned}$$

The real exponential can be compared with Beer’s Law, noting that intensity is proportional to the **square** of the wave function

$$\mu = 2\beta k \rightarrow \beta = \frac{\mu}{2k}$$

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$n = 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if'']$$

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$\begin{aligned}n &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if''] \\ &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f'] - i\frac{2\pi\rho_a r_0}{k^2} f''\end{aligned}$$

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$\begin{aligned}n &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if''] \\ &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f'] - i\frac{2\pi\rho_a r_0}{k^2} f'' \\ &= 1 - \delta\end{aligned}$$

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$\begin{aligned}n &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if''] \\&= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f'] - i\frac{2\pi\rho_a r_0}{k^2} f'' \\&= 1 - \delta + i\beta\end{aligned}$$

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$\begin{aligned}n &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if''] \\ &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f'] - i \frac{2\pi\rho_a r_0}{k^2} f'' \\ &= 1 - \delta + i\beta\end{aligned}$$

Since  $f^0(0) \gg f'$  in the forward direction, we have

$$\delta \approx \frac{2\pi\rho_a f^0(0)r_0}{k^2}$$

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$\begin{aligned}n &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if''] \\ &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f'] - i \frac{2\pi\rho_a r_0}{k^2} f'' \\ &= 1 - \delta + i\beta\end{aligned}$$

Since  $f^0(0) \gg f'$  in the forward direction, we have

$$\begin{aligned}\delta &\approx \frac{2\pi\rho_a f^0(0)r_0}{k^2} \\ \beta &= -\frac{2\pi\rho_a f''r_0}{k^2}\end{aligned}$$



## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$\begin{aligned}n &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if''] \\&= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f'] - i \frac{2\pi\rho_a r_0}{k^2} f'' \\&= 1 - \delta + i\beta\end{aligned}$$

Since  $f^0(0) \gg f'$  in the forward direction, we have

$$\begin{aligned}\delta &\approx \frac{2\pi\rho_a f^0(0)r_0}{k^2} \\ \beta &= -\frac{2\pi\rho_a f'' r_0}{k^2} = \frac{\mu}{2k}\end{aligned}$$

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$\begin{aligned}n &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if''] \\&= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f'] - i\frac{2\pi\rho_a r_0}{k^2} f'' \\&= 1 - \delta + i\beta\end{aligned}$$

Since  $f^0(0) \gg f'$  in the forward direction, we have

In terms of the absorption coefficient,  $\mu$

$$\begin{aligned}\delta &\approx \frac{2\pi\rho_a f^0(0)r_0}{k^2} \\ \beta &= -\frac{2\pi\rho_a f'' r_0}{k^2} = \frac{\mu}{2k} \\ f'' &= -\frac{k^2}{2\pi\rho_a r_0} \frac{\mu}{2k}\end{aligned}$$

## Absorption term in $n$

The absorptive term in the index of refraction is directly related to the  $f''$  term in the atomic scattering factor:

$$\begin{aligned}n &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f' + if''] \\ &= 1 - \frac{2\pi\rho_a r_0}{k^2} [f^0(Q) + f'] - i \frac{2\pi\rho_a r_0}{k^2} f'' \\ &= 1 - \delta + i\beta\end{aligned}$$

Since  $f^0(0) \gg f'$  in the forward direction, we have

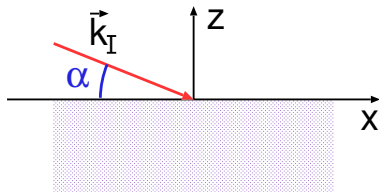
In terms of the absorption coefficient,  $\mu$ , and the atomic cross-section,  $\sigma_a$

$$\delta \approx \frac{2\pi\rho_a f^0(0)r_0}{k^2}$$
$$\beta = -\frac{2\pi\rho_a f'' r_0}{k^2} = \frac{\mu}{2k}$$

$$\begin{aligned}f'' &= -\frac{k^2}{2\pi\rho_a r_0} \frac{\mu}{2k} \\ &= -\frac{k}{4\pi r_0} \sigma_a\end{aligned}$$

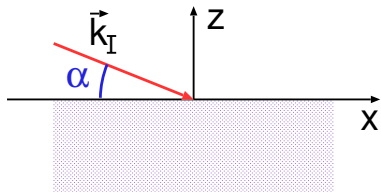
# Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



## Electromagnetic boundary conditions

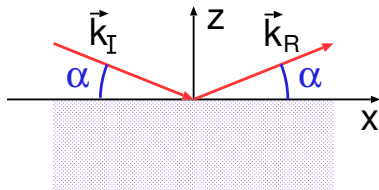
Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

# Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:

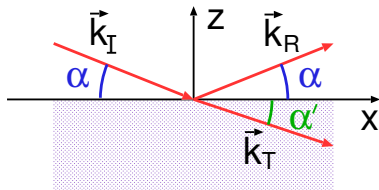


$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

$$\psi_R = a_R e^{i\vec{k}_R \cdot \vec{r}} \quad \text{reflected wave}$$

# Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



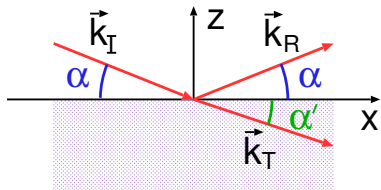
$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

$$\psi_R = a_R e^{i\vec{k}_R \cdot \vec{r}} \quad \text{reflected wave}$$

$$\psi_T = a_T e^{i\vec{k}_T \cdot \vec{r}} \quad \text{transmitted wave}$$

# Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

$$\psi_R = a_R e^{i\vec{k}_R \cdot \vec{r}} \quad \text{reflected wave}$$

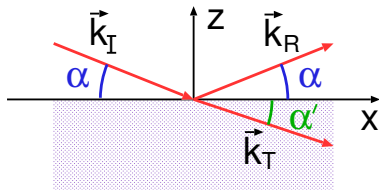
$$\psi_T = a_T e^{i\vec{k}_T \cdot \vec{r}} \quad \text{transmitted wave}$$

which leads to conditions on the amplitudes and the wave vectors of the waves at  $z = 0$ .



# Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

$$\psi_R = a_R e^{i\vec{k}_R \cdot \vec{r}} \quad \text{reflected wave}$$

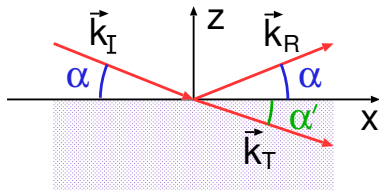
$$\psi_T = a_T e^{i\vec{k}_T \cdot \vec{r}} \quad \text{transmitted wave}$$

which leads to conditions on the amplitudes and the wave vectors of the waves at  $z = 0$ .

$$a_T = a_I + a_R$$

# Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

$$\psi_R = a_R e^{i\vec{k}_R \cdot \vec{r}} \quad \text{reflected wave}$$

$$\psi_T = a_T e^{i\vec{k}_T \cdot \vec{r}} \quad \text{transmitted wave}$$

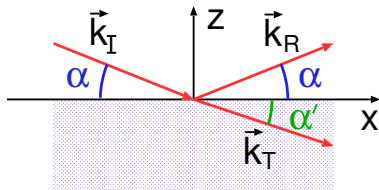
which leads to conditions on the amplitudes and the wave vectors of the waves at  $z = 0$ .

$$a_T = a_I + a_R$$

$$a_T \vec{k}_T = a_I \vec{k}_I + a_R \vec{k}_R$$

# Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

$$\psi_R = a_R e^{i\vec{k}_R \cdot \vec{r}} \quad \text{reflected wave}$$

$$\psi_T = a_T e^{i\vec{k}_T \cdot \vec{r}} \quad \text{transmitted wave}$$

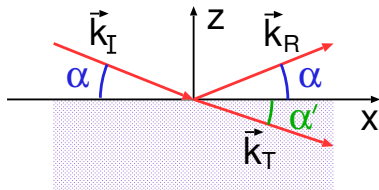
which leads to conditions on the amplitudes and the wave vectors of the waves at  $z = 0$ . Taking vector components:

$$a_T = a_I + a_R$$

$$a_T \vec{k}_T = a_I \vec{k}_I + a_R \vec{k}_R$$

## Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

$$\psi_R = a_R e^{i\vec{k}_R \cdot \vec{r}} \quad \text{reflected wave}$$

$$\psi_T = a_T e^{i\vec{k}_T \cdot \vec{r}} \quad \text{transmitted wave}$$

which leads to conditions on the amplitudes and the wave vectors of the waves at  $z = 0$ . Taking vector components:

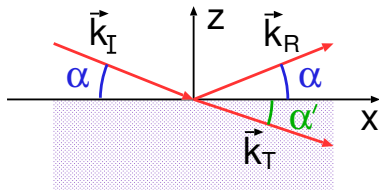
$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T = a_I + a_R$$

$$a_T \vec{k}_T = a_I \vec{k}_I + a_R \vec{k}_R$$

# Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:



$$\psi_I = a_I e^{i\vec{k}_I \cdot \vec{r}} \quad \text{incident wave}$$

$$\psi_R = a_R e^{i\vec{k}_R \cdot \vec{r}} \quad \text{reflected wave}$$

$$\psi_T = a_T e^{i\vec{k}_T \cdot \vec{r}} \quad \text{transmitted wave}$$

which leads to conditions on the amplitudes and the wave vectors of the waves at  $z = 0$ . Taking vector components:

$$a_T = a_I + a_R$$

$$a_T \vec{k}_T = a_I \vec{k}_I + a_R \vec{k}_R$$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$



## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T nk \cos \alpha' = a_I k \cos \alpha + a_R k \cos \alpha$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

Combining with the amplitude equation and cancelling  $k$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T nk \cos \alpha' = a_I k \cos \alpha + a_R k \cos \alpha$$

$$a_T = a_I + a_R$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

Combining with the amplitude equation and cancelling  $k$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T nk \cos \alpha' = a_I k \cos \alpha + a_R k \cos \alpha$$

$$a_T = a_I + a_R$$

$$(a_I + a_R)n \cos \alpha' = (a_I + a_R) \cos \alpha$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

Combining with the amplitude equation and cancelling  $k$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T nk \cos \alpha' = a_I k \cos \alpha + a_R k \cos \alpha$$

$$a_T = a_I + a_R$$

This simply results in Snell's Law

$$(a_I + a_R)n \cos \alpha' = (a_I + a_R) \cos \alpha$$

$$\cos \alpha = n \cos \alpha'$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

Combining with the amplitude equation and cancelling  $k$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T nk \cos \alpha' = a_I k \cos \alpha + a_R k \cos \alpha$$

$$a_T = a_I + a_R$$

This simply results in Snell's Law which for small angles can be expanded.

$$(a_I + a_R)n \cos \alpha' = (a_I + a_R) \cos \alpha$$

$$\cos \alpha = n \cos \alpha'$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

Combining with the amplitude equation and cancelling  $k$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T nk \cos \alpha' = a_I k \cos \alpha + a_R k \cos \alpha$$

$$a_T = a_I + a_R$$

This simply results in Snell's Law which for small angles can be expanded.

$$(a_I + a_R)n \cos \alpha' = (a_I + a_R) \cos \alpha$$

$$\cos \alpha = n \cos \alpha'$$

$$1 - \frac{\alpha^2}{2} = (1 - \delta + i\beta) \left(1 - \frac{\alpha'^2}{2}\right)$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

Combining with the amplitude equation and cancelling  $k$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T nk \cos \alpha' = a_I k \cos \alpha + a_R k \cos \alpha$$

$$a_T = a_I + a_R$$

This simply results in Snell's Law which for small angles can be expanded.

$$(a_I + a_R)n \cos \alpha' = (a_I + a_R) \cos \alpha$$

$$\cos \alpha = n \cos \alpha'$$

$$1 - \frac{\alpha^2}{2} = (1 - \delta + i\beta) \left( 1 - \frac{\alpha'^2}{2} \right)$$

$$-\alpha^2 = -\alpha'^2 - 2\delta + 2i\beta$$

## Parallel projection & Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

$$|\vec{k}_R| = |\vec{k}_I| = k \quad \text{in vacuum}$$

$$|\vec{k}_T| = nk \quad \text{in medium}$$

Combining with the amplitude equation and cancelling  $k$

$$a_T k_T \cos \alpha' = a_I k_I \cos \alpha + a_R k_R \cos \alpha$$

$$a_T nk \cos \alpha' = a_I k \cos \alpha + a_R k \cos \alpha$$

$$a_T = a_I + a_R$$

This simply results in Snell's Law which for small angles can be expanded.

$$(a_I + a_R)n \cos \alpha' = (a_I + a_R) \cos \alpha$$

$$\cos \alpha = n \cos \alpha'$$

$$1 - \frac{\alpha^2}{2} = (1 - \delta + i\beta) \left(1 - \frac{\alpha'^2}{2}\right)$$

$$-\alpha^2 = -\alpha'^2 - 2\delta + 2i\beta$$

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

Recalling that

$$\alpha_c = \sqrt{2\delta}$$



# Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors

$$\begin{aligned} -a_T k_T \sin \alpha' &= -a_I k_I \sin \alpha + a_R k_R \sin \alpha \\ -a_T n k \sin \alpha' &= -(a_I - a_R) k \sin \alpha \end{aligned}$$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha}$$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha} \approx n \frac{\alpha'}{\alpha}$$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha} \approx n \frac{\alpha'}{\alpha} \approx \frac{\alpha'}{\alpha}$$

taking  $n \approx 1$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha} \approx n \frac{\alpha'}{\alpha} \approx \frac{\alpha'}{\alpha}$$

taking  $n \approx 1$

The Fresnel Equations  
can now be derived



## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha} \approx n \frac{\alpha'}{\alpha} \approx \frac{\alpha'}{\alpha}$$

taking  $n \approx 1$

$$a_I \alpha - a_R \alpha = a_I \alpha' + a_R \alpha'$$

The Fresnel Equations  
can now be derived

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha} \approx n \frac{\alpha'}{\alpha} \approx \frac{\alpha'}{\alpha}$$

taking  $n \approx 1$

The Fresnel Equations  
can now be derived

$$a_I \alpha - a_R \alpha = a_I \alpha' + a_R \alpha'$$

$$a_I (\alpha - \alpha') = a_R (\alpha + \alpha')$$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha} \approx n \frac{\alpha'}{\alpha} \approx \frac{\alpha'}{\alpha}$$

taking  $n \approx 1$

$$a_I \alpha - a_R \alpha = a_I \alpha' + a_R \alpha'$$

$$a_I (\alpha - \alpha') = a_R (\alpha + \alpha') \rightarrow r$$

The Fresnel Equations  
can now be derived

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha} \approx n \frac{\alpha'}{\alpha} \approx \frac{\alpha'}{\alpha}$$

taking  $n \approx 1$

The Fresnel Equations  
can now be derived

$$a_I \alpha - a_R \alpha = a_I \alpha' + a_R \alpha'$$

$$a_I (\alpha - \alpha') = a_R (\alpha + \alpha') \rightarrow r$$

$$a_I (\alpha - \alpha') = (a_T - a_I) (\alpha + \alpha')$$

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$

## Perpendicular projection & Fresnel equations

Taking the perpendicular projection, substituting for the wave vectors and using the amplitude equation

$$a_T = a_I + a_R$$

$$-a_T k_T \sin \alpha' = -a_I k_I \sin \alpha + a_R k_R \sin \alpha$$

$$-a_T n k \sin \alpha' = -(a_I - a_R) k \sin \alpha$$

$$(a_I + a_R) n \sin \alpha' = (a_I - a_R) \sin \alpha$$

$$\frac{a_I - a_R}{a_I + a_R} = \frac{n \sin \alpha'}{\sin \alpha} \approx n \frac{\alpha'}{\alpha} \approx \frac{\alpha'}{\alpha}$$

taking  $n \approx 1$

The Fresnel Equations can now be derived

$$a_I \alpha - a_R \alpha = a_I \alpha' + a_R \alpha'$$

$$a_I (\alpha - \alpha') = a_R (\alpha + \alpha') \rightarrow r$$

$$a_I (\alpha - \alpha') = (a_T - a_I) (\alpha + \alpha') \rightarrow t$$

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$

$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

## Reflectivity and transmittivity

$r$  and  $t$  are called the reflection and transmission coefficients, respectively.

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$
$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

## Reflectivity and transmittivity

$r$  and  $t$  are called the reflection and transmission coefficients, respectively. The reflectivity  $R = |r|^2$  and transmittivity  $T = |t|^2$  are the squares of these quantities, which are complex because  $\alpha'$  is complex.

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$
$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

## Reflectivity and transmittivity

$r$  and  $t$  are called the reflection and transmission coefficients, respectively. The reflectivity  $R = |r|^2$  and transmittivity  $T = |t|^2$  are the squares of these quantities, which are complex because  $\alpha'$  is complex.

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$
$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

$$\alpha' = \text{Re}(\alpha') + i \text{Im}(\alpha')$$



## Reflectivity and transmittivity

$r$  and  $t$  are called the reflection and transmission coefficients, respectively. The reflectivity  $R = |r|^2$  and transmittivity  $T = |t|^2$  are the squares of these quantities, which are complex because  $\alpha'$  is complex.

$$\alpha' = \text{Re}(\alpha') + i \text{Im}(\alpha')$$

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$
$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

In the  $z$  direction, the amplitude of the transmitted wave has two terms

## Reflectivity and transmittivity

$r$  and  $t$  are called the reflection and transmission coefficients, respectively. The reflectivity  $R = |r|^2$  and transmittivity  $T = |t|^2$  are the squares of these quantities, which are complex because  $\alpha'$  is complex.

$$\alpha' = \text{Re}(\alpha') + i \text{Im}(\alpha')$$

$$a_T e^{ik\alpha'z} = a_T e^{ik \text{Re}(\alpha')z} e^{-k \text{Im}(\alpha')z}$$

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$
$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

In the  $z$  direction, the amplitude of the transmitted wave has two terms

## Reflectivity and transmittivity

$r$  and  $t$  are called the reflection and transmission coefficients, respectively. The reflectivity  $R = |r|^2$  and transmittivity  $T = |t|^2$  are the squares of these quantities, which are complex because  $\alpha'$  is complex.

$$\alpha' = \text{Re}(\alpha') + i \text{Im}(\alpha')$$

$$a_T e^{ik\alpha'z} = a_T e^{ik \text{Re}(\alpha')z} e^{-k \text{Im}(\alpha')z}$$

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$
$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

In the  $z$  direction, the amplitude of the transmitted wave has two terms with the second one being the attenuation of the wave in the medium due to absorption.

## Reflectivity and transmittivity

$r$  and  $t$  are called the reflection and transmission coefficients, respectively. The reflectivity  $R = |r|^2$  and transmittivity  $T = |t|^2$  are the squares of these quantities, which are complex because  $\alpha'$  is complex.

$$\alpha' = \text{Re}(\alpha') + i \text{Im}(\alpha')$$

$$a_T e^{ik\alpha'z} = a_T e^{ik \text{Re}(\alpha')z} e^{-k \text{Im}(\alpha')z}$$

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$
$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

In the  $z$  direction, the amplitude of the transmitted wave has two terms with the second one being the attenuation of the wave in the medium due to absorption. This attenuation is characterized by a quantity called the penetration depth,  $\Lambda$ .

## Reflectivity and transmittivity

$r$  and  $t$  are called the reflection and transmission coefficients, respectively. The reflectivity  $R = |r|^2$  and transmittivity  $T = |t|^2$  are the squares of these quantities, which are complex because  $\alpha'$  is complex.

$$\alpha' = \text{Re}(\alpha') + i \text{Im}(\alpha')$$

$$a_T e^{ik\alpha'z} = a_T e^{ik \text{Re}(\alpha')z} e^{-k \text{Im}(\alpha')z}$$

$$\Lambda = \frac{1}{2k \text{Im}(\alpha')}$$

$$r = \frac{a_R}{a_I} = \frac{\alpha - \alpha'}{\alpha + \alpha'}$$
$$t = \frac{a_T}{a_I} = \frac{2\alpha}{\alpha + \alpha'}$$

In the  $z$  direction, the amplitude of the transmitted wave has two terms with the second one being the attenuation of the wave in the medium due to absorption. This attenuation is characterized by a quantity called the penetration depth,  $\Lambda$ .

## Wavevector transfers

While it is physically easier to think of angles, a more useful parameter is called the wavevector transfer.

## Wavevector transfers

While it is physically easier to think of angles, a more useful parameter is called the wavevector transfer.

$$Q = 2k \sin \alpha \approx 2k\alpha$$

## Wavevector transfers

While it is physically easier to think of angles, a more useful parameter is called the wavevector transfer.

$$Q = 2k \sin \alpha \approx 2k\alpha$$

and for the critical angle

$$Q_c = 2k \sin \alpha_c \approx 2k\alpha_c$$



## Wavevector transfers

While it is physically easier to think of angles, a more useful parameter is called the wavevector transfer.

$$Q = 2k \sin \alpha \approx 2k\alpha$$

and for the critical angle

$$Q_c = 2k \sin \alpha_c \approx 2k\alpha_c$$

in dimensionless units, these become

## Wavevector transfers

While it is physically easier to think of angles, a more useful parameter is called the wavevector transfer.

$$Q = 2k \sin \alpha \approx 2k\alpha$$

and for the critical angle

$$Q_c = 2k \sin \alpha_c \approx 2k\alpha_c$$

in dimensionless units, these become

$$q = \frac{Q}{Q_c} \approx \frac{2k}{2k} \alpha$$

## Wavevector transfers

While it is physically easier to think of angles, a more useful parameter is called the wavevector transfer.

$$Q = 2k \sin \alpha \approx 2k\alpha$$

and for the critical angle

$$Q_c = 2k \sin \alpha_c \approx 2k\alpha_c$$

in dimensionless units, these become

$$q = \frac{Q}{Q_c} \approx \frac{2k}{Q_c} \alpha \quad q' = \frac{Q'}{Q_c} \approx \frac{2k}{Q_c} \alpha'$$

$q$  is a convenient parameter to use because it is a combination of two parameters which are often varied in experiments, the angle of incidence  $\alpha$  and the wavenumber (energy) of the x-ray,  $k$ .

## Defining equations in $q$

Start with the reduced version of Snell's Law

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

## Defining equations in $q$

Start with the reduced version of Snell's Law and multiply by a  $1/\alpha_c^2 = (2k/Q_c)^2$ .

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

## Defining equations in $q$

Start with the reduced version of Snell's Law and multiply by a  $1/\alpha_c^2 = (2k/Q_c)^2$ .

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

$$\left(\frac{2k}{Q_c}\right)^2 \alpha^2 = \left(\frac{2k}{Q_c}\right)^2 (\alpha'^2 + \alpha_c^2 - 2i\beta)$$

## Defining equations in $q$

Start with the reduced version of Snell's Law and multiply by a  $1/\alpha_c^2 = (2k/Q_c)^2$ .

Noting that

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

$$q = \frac{2k}{Q_c} \alpha$$

$$\left(\frac{2k}{Q_c}\right)^2 \alpha^2 = \left(\frac{2k}{Q_c}\right)^2 (\alpha'^2 + \alpha_c^2 - 2i\beta)$$

## Defining equations in $q$

Start with the reduced version of Snell's Law and multiply by a  $1/\alpha_c^2 = (2k/Q_c)^2$ .

Noting that

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

$$q = \frac{2k}{Q_c} \alpha$$

$$\left(\frac{2k}{Q_c}\right)^2 \alpha^2 = \left(\frac{2k}{Q_c}\right)^2 (\alpha'^2 + \alpha_c^2 - 2i\beta)$$

$$\begin{aligned} \left(\frac{2k}{Q_c}\right)^2 \beta &= \frac{4k^2}{Q_c^2} \frac{\mu}{2k} \\ &= \frac{2k}{Q_c^2} \mu = b_\mu \end{aligned}$$



## Defining equations in $q$

Start with the reduced version of Snell's Law and multiply by a  $1/\alpha_c^2 = (2k/Q_c)^2$ .

Noting that

$$q = \frac{2k}{Q_c} \alpha$$

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

$$\left(\frac{2k}{Q_c}\right)^2 \alpha^2 = \left(\frac{2k}{Q_c}\right)^2 (\alpha'^2 + \alpha_c^2 - 2i\beta)$$

$$\begin{aligned} \left(\frac{2k}{Q_c}\right)^2 \beta &= \frac{4k^2}{Q_c^2} \frac{\mu}{2k} \\ &= \frac{2k}{Q_c^2} \mu = b_\mu \end{aligned}$$

$$q^2 = q'^2 + 1 - 2ib_\mu$$

## Defining equations in $q$

Start with the reduced version of Snell's Law and multiply by a  $1/\alpha_c^2 = (2k/Q_c)^2$ .

Noting that

$$q = \frac{2k}{Q_c} \alpha$$

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

$$\left(\frac{2k}{Q_c}\right)^2 \alpha^2 = \left(\frac{2k}{Q_c}\right)^2 (\alpha'^2 + \alpha_c^2 - 2i\beta)$$

$$\begin{aligned} \left(\frac{2k}{Q_c}\right)^2 \beta &= \frac{4k^2}{Q_c^2} \frac{\mu}{2k} \\ &= \frac{2k}{Q_c^2} \mu = b_\mu \end{aligned}$$

$$q^2 = q'^2 + 1 - 2ib_\mu$$

Similarly, we convert the reflection and transmission coefficients.

## Defining equations in $q$

Start with the reduced version of Snell's Law and multiply by a  $1/\alpha_c^2 = (2k/Q_c)^2$ .

Noting that

$$\alpha^2 = \alpha'^2 + \alpha_c^2 - 2i\beta$$

$$q = \frac{2k}{Q_c} \alpha$$

$$\left(\frac{2k}{Q_c}\right)^2 \alpha^2 = \left(\frac{2k}{Q_c}\right)^2 (\alpha'^2 + \alpha_c^2 - 2i\beta)$$

$$\begin{aligned} \left(\frac{2k}{Q_c}\right)^2 \beta &= \frac{4k^2}{Q_c^2} \frac{\mu}{2k} \\ &= \frac{2k}{Q_c^2} \mu = b_\mu \end{aligned}$$

$$q^2 = q'^2 + 1 - 2ib_\mu$$

Similarly, we convert the reflection and transmission coefficients.

$$r = \frac{q - q'}{q + q'}$$

$$t = \frac{2q}{q + q'}$$