## Today's Outline - September 26, 2016

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- Reflectivity research topics


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APS Visits:
10-ID: Friday, October 21, 2016
10-BM: Friday, October 28, 2016

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Homework Assignment \#03:
Chapter 3: 1, 3, 4, 6, 8
due Wednesday, October 05, 2016

## Layering in liquid films

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ethylhexoxy)-silane,
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A broad peak appears at free surface indicating that ordering requires a hard smooth surface.

## Film growth kinetics

Gaussian roughness profile with a "roughness" exponent $0<h<1$.

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Thus $z_{s}=h / \beta=2.7$ and diffraction data confirm $\xi=19.9\langle h\rangle^{1 / 2.7} \AA$

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P. Pershan, "Review of the highlights of $x$-ray studies of liquid metal surfaces", J. Appl. Phys. 116, 222201 (2014).

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High vapor pressure and thermal excitations limit the number of pure metals which can be studied but alloy eutectics provide many possibilities

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surface layer is rich in Bi (95\%), second layer is deficient ( $25 \%$ ), and third layer is rich in $\mathrm{Bi}(53 \%)$ once again

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## The MRCAT mirror



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A mounting system which permits angular positioning to less than $1 / 100$ of a degree as well as horizontal and vertical motions

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One platinum stripe and one rhodium stripe deposited along the length of the mirror on top of a chromium buffer layer

A mounting system which permits angular positioning to less than $1 / 100$ of a degree as well as horizontal and vertical motions

A bending mechanism to permit vertical focusing of the beam to $\sim 60 \mu \mathrm{~m}$

## Mirror performance

When illuminated with 12 keV $x$-rays on the glass "stripe", the reflectivity is measured as:


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As energy rises, the Pt layer begins to show the reflectivity of a thin slab.

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A cost effective way to focus in both directions is a toroidal mirror which has a fixed bend in the transverse direction
 but which can be bent longitudinally to change the vertical focus.

## Dual focusing options

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## Dual focusing options

- Toroidal mirror - simple, moderate focus, good for initial focusing element, easy to distort beam
- Saggittal focusing crystal \& vertical focusing mirror adjustable in both directions, good for initial focusing element
- Kirkpatrick-Baez mirror pair - in combination with an initial focusing element, good for final small focal spot and variable energy
- K-B mirrors \& zone plates - in combination with an initial focusing element, gives smallest focal spot, but hard to vary energy


## Refractive optics

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x-ray lenses are complementary to those for visible light getting manageable focal distances requires making compound lenses


## Focal length of a compound lens

## Start with a 3-element compound lens, calculate effective focal length

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\frac{1}{i_{1}}=\frac{1}{f_{1}}-\frac{1}{o_{1}} \rightarrow \frac{1}{i_{1}}=\frac{1}{f}
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Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length, $f$

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for the second lens, the image $i_{1}$ is a virtual object, $o_{2}=-i_{1}$

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\frac{1}{i_{2}}=\frac{1}{f_{2}}-\frac{1}{o_{2}} \rightarrow \frac{1}{i_{2}}=\frac{1}{f}+\frac{1}{f}
\end{gathered}
$$

Start with a 3-element compound lens, calculate effective focal length assuming each lens has the same focal length, $f$

$$
f_{1}=f, o_{1}=\infty
$$

for the second lens, the image $i_{1}$ is a virtual object, $o_{2}=-i_{1}$

## Focal length of a compound lens

$$
\begin{gathered}
\longrightarrow \\
\frac{1}{i}+\frac{1}{o}=\frac{1}{f} \rightarrow \frac{1}{i}=\frac{1}{f}-\frac{1}{o} \\
\frac{1}{i_{1}}=\frac{1}{f_{1}}-\frac{1}{o_{1}} \rightarrow \frac{1}{i_{1}}=\frac{1}{f} \rightarrow i_{1}=f \\
\frac{1}{i_{2}}=\frac{1}{f_{2}}-\frac{1}{o_{2}} \rightarrow \frac{1}{i_{2}}=\frac{1}{f}+\frac{1}{f} \rightarrow i_{2}=\frac{f}{2}
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\frac{1}{i_{2}}=\frac{1}{f_{2}}-\frac{1}{o_{2}} \rightarrow \frac{1}{i_{2}}=\frac{1}{f}+\frac{2}{f} \rightarrow i_{2}=\frac{f}{3}
\end{gathered}
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## Focal length of a compound lens

$\longrightarrow \begin{aligned} & \text { Start with a 3-element } \\ & \text { compound lens, calculate } \\ & \text { effective focal length } \\ & \text { assuming each lens has } \\ & \text { the same focal length, } f\end{aligned}$
$\frac{1}{i}+\frac{1}{o}=\frac{1}{f} \rightarrow \frac{1}{i}=\frac{1}{f}-\frac{1}{o}=\frac{1}{f_{1}}-\frac{1}{o_{1}} \rightarrow \frac{1}{i_{1}}=\frac{1}{f} \rightarrow i_{1}=f, o_{1}=\infty$
$\frac{1}{i_{1}}=\frac{1}{f_{2}}-\frac{1}{o_{2}} \rightarrow \frac{1}{i_{2}}=\frac{1}{f}+\frac{1}{f} \rightarrow i_{2}=\frac{f}{2}$
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object, the second lens, the is $o_{1}=-i_{1}$ $\begin{aligned} & \text { similarly for the third lens, } \\ & o_{3}=-i_{2}\end{aligned}$

## Rephasing distance

A spherical surface is not the ideal lens as it introduces aberrations. Derive the ideal shape for perfect focusing of $x$-rays.

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$$
\begin{aligned}
& \text { consider two waves, one traveling in- } \\
& \text { side the solid and the other in vacuum, } \\
& \lambda=\lambda_{0} /(1-\delta) \approx \lambda_{0}(1+\delta)
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> consider two waves, one traveling inside the solid and the other in vacuum, $\lambda=\lambda_{0} /(1-\delta) \approx \lambda_{0}(1+\delta)$
if the two waves start in phase, they will be in phase once again after a distance

$$
\Lambda=(N+1) \lambda_{0}=N \lambda_{0}(1+\delta)
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| $\uparrow$ | $\uparrow$ | consider two waves, one traveling inside the solid and the other in vacuum, $\lambda=\lambda_{0} /(1-\delta) \approx \lambda_{0}(1+\delta)$ |
| :---: | :---: | :---: |
|  | $\Lambda$ | if the two waves start in phase, they will be in phase once again after a distance |
| $\lambda_{\text {o }}$ | $\lambda_{0}(1+\delta)$ | $\Lambda=(N+1) \lambda_{0}=N \lambda_{0}(1+\delta)$ |
|  | $N \lambda_{0}+\lambda_{0}$ | $+N \delta \lambda_{0}$ |

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| :--- |
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| :--- |
| once again after a distance |

$N=(N+1) \lambda_{0}=N \lambda_{0}(1+\delta)$
$N \lambda_{0}+\lambda_{0}=N \lambda_{0}+N \delta \lambda_{0} \longrightarrow \lambda_{0}=N \delta \lambda_{0}$

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| $\lambda_{0}$ |
| :--- |
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| :--- |
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## Ideal interface profile



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The wave exits the material into vacuum through a surface of profile $h(x)$, and is twisted by an angle $\alpha$.

## Ideal interface profile



The wave exits the material into vacuum through a surface of profile $h(x)$, and is twisted by an angle $\alpha$. Follow the path of two points on the wavefront, $A$ and $A^{\prime}$ as they propagate to $B$ and $B^{\prime}$.

## Ideal interface profile


from the $A A^{\prime} B^{\prime}$ triangle

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\lambda_{0}(1+\delta)=h^{\prime}(x) \Delta x
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\lambda_{0}(1+\delta)=h^{\prime}(x) \Delta x \longrightarrow \Delta x \approx \frac{\lambda_{0}}{h^{\prime}(x)}
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from the $A A^{\prime} B^{\prime}$ triangle
and from the $B C B^{\prime}$ tri-

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and from the $B C B^{\prime}$ triangle using $\Lambda=\lambda_{0} / \delta$

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\alpha(x) \approx \frac{\lambda_{0} \delta}{\Delta x}=h^{\prime}(x) \delta=h^{\prime}(x) \frac{\lambda_{0}}{\Lambda}
\end{array}
$$

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$$
\frac{h(x)}{\Lambda}=\frac{x^{2}}{2 f \lambda_{0}}=\left[\frac{x}{\sqrt{2 f \lambda_{0}}}\right]^{2}
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$$


a parabola is the ideal surface for focusing be refraction


[^0]:    P. Pershan, "Review of the highlights of x-ray studies of liquid metal surfaces", J. Appl. Phys. 116, 222201 (2014).

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