## Today's Outline - February 12, 2015

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- Homework \#02 discussion


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- Reflection from a graded index


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- Reflection from a graded index
- Reflection from rough interfaces and surfaces
- Models of Surfaces
- Reflectivity from the MRCAT mirror


## HW \#02

1. Knowing that the photoelectric absorption of an element scales as the inverse of the energy cubed, calculate:
(a) the absorption coefficient at 10 keV for copper when the value at 5 keV is $1698.3 \mathrm{~cm}^{-1}$;
(b) The actual absorption coefficient of copper at 10 keV is $1942.1 \mathrm{~cm}^{-1}$, why is this so different than your calculated value?
2. A 30 cm long, ionization chamber, filled with $80 \%$ helium and $20 \%$ nitrogen gases at 1 atmosphere, is being used to measure the photon rate (photons $/ \mathrm{sec}$ ) in a synchrotron beamline at 12 keV . If a current of 10 nA is measured, what is the photon flux entering the ionization chamber?
3. A 5 cm deep ionization chamber is used to measure the fluorescence from a sample containing arsenic (As). Using any noble gases or nitrogen, determine a gas fill (at 1 atmosphere) for this chamber which absorbs at least $60 \%$ of the incident photons. How does this change if you are measuring the fluorescence from ruthenium ( Ru ) ?

## HW \#02

4. Calculate the critical angle of reflection of 10 keV and 30 keV x-rays for:
(a) A slab of glass $\left(\mathrm{SiO}_{2}\right)$;
(b) A thick chromium mirror;
(c) A thick platinum mirror.
(d) If the incident x-ray beam is 2 mm high, what length of mirror is required to reflect the entire beam for each material?
5. Calculate the fraction of silver $(\mathrm{Ag})$ fluorescence x -rays which are absorbed in a 1 mm thick silicon ( Si ) detector and the charge pulse expected for each absorbed photon. Repeat the calculation for a 1 mm thick germanium ( Ge ) detector.

## Graded Interfaces

Since most interfaces are not sharp, it is important to be able to model a graded interface, where the density, and therefore the index of refraction varies near the interface itself.

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The density profile of the interface can be described by the function $f(z)$ which approaches 1 as $z \rightarrow \infty$.

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The density profile of the interface can be described by the function $f(z)$ which approaches 1 as $z \rightarrow \infty$.

The reflectivity can be computed as the superposition of the reflectivity of a series of infinitesmal slabs of thickness $d z$ at a depth $z$.

## Reflectivity of a Graded Interface

> The differential reflectivity from a slab of thickness $d z$ at depth $z$ is:

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integrating by parts simplifies the term in front is simply the Fresnel reflectivity for an interface, $r_{F}(Q)$ when $q \gg 1$, the integral is the Fourier transform of the density gradient, $\phi(Q)$

Calculating the full reflection coefficient relative to the Fresnel reflection coefficient

$$
\frac{R(Q)}{R_{F}(Q)}=\left|\int_{-\infty}^{\infty}\left(\frac{d f}{d z}\right) e^{i Q z} d z\right|^{2}
$$

## The Error Function - a Specific Case

The error function is often chosen as a model for the density gradient

$$
f(z)=\operatorname{erf}\left(\frac{z}{\sqrt{2} \sigma}\right)=\frac{1}{\sqrt{\pi}} \int_{0}^{z / \sqrt{2} \sigma} e^{-t^{2}} d t
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whose Fourier transform is also a Gaussian, which when squared to obtain the reflection coefficient, gives.

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R(Q)=R_{F}(Q) e^{-Q^{2} \sigma^{2}}
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R(Q)=R_{F}(Q) e^{-Q^{2} \sigma^{2}}=R_{F}(Q) e^{-Q Q^{\prime} \sigma^{2}}
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whose Fourier transform is also a Gaussian, which when squared to obtain the reflection coefficient, gives. Or more accurately.

$$
\begin{gathered}
R(Q)=R_{F}(Q) e^{-Q^{2} \sigma^{2}}=R_{F}(Q) e^{-Q Q^{\prime} \sigma^{2}} \\
Q=k \sin \theta, \quad Q^{\prime}=k^{\prime} \sin \theta^{\prime}
\end{gathered}
$$

## Rough Surfaces

When a surface or interface is not perfectly smooth but has some roughness the reflectivity is no longer simply specular but has a non-zero diffuse component which we must include in the model.

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r_{V}=-r_{0} \int_{V}(\rho d \vec{r}) e^{i \vec{Q} \cdot \vec{r}}
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The incident and scattered angles are no longer the same, the x-rays illuminate the volume $V$. The scattering from the entire, illuminated volume is given by using Gauss' theorem.
$\int_{V}(\vec{\nabla} \cdot \vec{C}) d \vec{r}=\int_{S} \vec{C} \cdot d \vec{S}$

## Conversion to Surface Integral

$$
\int_{V}(\vec{\nabla} \cdot \vec{C}) d \vec{r}=\int_{S} \vec{C} \cdot d \vec{S}
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Taking

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$$
=-r_{o} \rho \int_{V} \vec{\nabla} \cdot\left(\hat{z} \frac{e^{i \vec{Q} \cdot \vec{r}}}{i Q_{z}}\right) \cdot d \vec{r}
$$

We have

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We have

$$
\begin{aligned}
& =-r_{o} \rho \int_{V} \vec{\nabla} \cdot\left(\hat{z} \frac{e^{i \vec{Q} \cdot \vec{r}}}{i Q_{z}}\right) \cdot d \vec{r} \\
r_{S} & =-r_{o} \rho \int_{S}\left(\hat{z} \frac{e^{i \vec{Q} \cdot \vec{r}}}{i Q_{z}}\right) \cdot d \vec{S}
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$$
r_{S}=-r_{o} \rho \frac{1}{i Q_{z}} \int_{S} e^{i \vec{Q} \cdot \vec{r}} d x d y
$$

## Evaluation of Surface Integral

The side surfaces of the volume do not contribute to this integral as they are along the $\hat{z}$ direction, but we can also choose the thickness of the slab such that the lower surface will not contribute either.

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r_{S}=-\frac{r_{o} \rho}{i Q_{z}} \int_{S} e^{i Q_{z} h(x, y)} e^{i\left(Q_{x} x+Q_{y} y\right)} d x d y
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$$

The actual scattering cross section is the square of this integral

$$
\frac{d \sigma}{d \Omega}=\left(\frac{r_{0} \rho}{Q_{z}}\right)^{2} \int_{S} \int_{S^{\prime}} e^{i Q_{z}\left(h(x, y)-h\left(x^{\prime}, y^{\prime}\right)\right)} e^{i Q_{x}\left(x-x^{\prime}\right)} e^{i Q_{y}\left(y-y^{\prime}\right)} d x d y d x^{\prime} d y^{\prime}
$$

## Scattering Cross Section

If we assume that $h(x, y)-h\left(x^{\prime}, y^{\prime}\right)$ depends only on the relative difference in position, $x-x^{\prime}$ and $y-y^{\prime}$ the four dimensional integral collapses to the product of two two dimensional integrals

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\left(\frac{d \sigma}{d \Omega}\right)=\left(\frac{r_{0} \rho}{Q_{z}}\right)^{2} \int_{S^{\prime}} d x^{\prime} d y^{\prime} \int_{S}\left\langle e^{i Q_{z}(h(0,0)-h(x, y))}\right\rangle e^{i Q_{x} x} e^{i Q_{y} y} d x d y
$$

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& =\left(\frac{r_{o} \rho}{Q_{z}}\right)^{2} \frac{A_{o}}{\sin \theta_{1}} \int\left\langle e^{i Q_{z}(h(0,0)-h(x, y))}\right\rangle e^{i Q_{x} x} e^{i Q_{y} y} d x d y
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where $A_{o} / \sin \theta_{1}$ is just the illuminated surface area

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where $A_{o} / \sin \theta_{1}$ is just the illuminated surface area and the term in the angled brackets is an ensemble average over all possible choices of the origin within the illuminated area.

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\end{aligned}
$$

where $A_{o} / \sin \theta_{1}$ is just the illuminated surface area and the term in the angled brackets is an ensemble average over all possible choices of the origin within the illuminated area.
Finally, it is assumed that the statistics of the height variation are Gaussian and

$$
\left(\frac{d \sigma}{d \Omega}\right)=\left(\frac{r_{o} \rho}{Q_{z}}\right)^{2} \frac{A_{o}}{\sin \theta_{1}} \int e^{-Q_{z}^{2}\left\langle[h(0,0)-h(x, y)]^{2}\right\rangle / 2} e^{i Q_{x} x} e^{i Q_{y} y} d x d y
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2 \pi \delta(q)=\int e^{i q x} d x \quad\left(\frac{d \sigma}{d \Omega}\right)=\left(\frac{r_{o} \rho}{Q_{z}}\right)^{2} \frac{A_{o}}{\sin \theta_{1}} \int e^{i Q_{x} x} e^{i Q_{y} y} d x d y
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R\left(Q_{z}\right)=\frac{I_{s c}}{I_{0}}=\left(\frac{Q_{c}^{2} / 8}{Q_{z}}\right)^{2}\left(\frac{1}{Q_{z} / 2}\right)^{2}=\left(\frac{Q_{c}}{2 Q_{z}}\right)^{4}
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And the scattering exhibits both a specular peak, reduced by uncorrelated roughness, and diffuse scattering from the correlated portion of the surface

## The MRCAT Mirror



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Ultra low expansion glass polished to a few Å roughness

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A bending mechanism to permit vertical focusing of the beam to $\sim 60 \mu \mathrm{~m}$

## Mirror Performance I

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As energy rises, the Pt layer begins to show the reflectivity of a thin slab.

