## Today's Outline - February 03, 2015

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- Refraction and reflection


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- Boundary conditions at an interface


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- Refraction and reflection
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Reading Assignment: Chapter 3.4

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- Refraction and reflection
- Boundary conditions at an interface
- The Fresnel equations
- Reflectivity and Transmittivity
- Normalized $q$-coordinates

Reading Assignment: Chapter 3.4
Homework Assignment \#02:
Problems to be provided
due Thursday, February 12, 2015

## HW \#02

1. Knowing that the photoelectric absorption of an element scales as the inverse of the energy cubed, calculate:
(a) the absorption coefficient at 10 keV for copper when the value at 5 keV is $1698.3 \mathrm{~cm}^{-1}$;
(b) The actual absorption coefficient of copper at 10 keV is $1942.1 \mathrm{~cm}^{-1}$, why is this so different than your calculated value?
2. A 30 cm long, ionization chamber, filled with $80 \%$ helium and $20 \%$ nitrogen gases at 1 atmosphere, is being used to measure the photon rate (photons $/ \mathrm{sec}$ ) in a synchrotron beamline at 12 keV . If a current of 10 nA is measured, what is the photon flux entering the ionization chamber?
3. A 5 cm deep ionization chamber is used to measure the fluorescence from a sample containing arsenic (As). Using any noble gases or nitrogen, determine a gas fill (at 1 atmosphere) for this chamber which absorbs at least $60 \%$ of the incident photons. How does this change if you are measuring the fluorescence from ruthenium ( Ru ) ?

## HW \#02

4. Calculate the characteristic angle of reflection of 10 keV and 30 keV $x$-rays for:
(a) A slab of glass $\left(\mathrm{SiO}_{2}\right)$;
(b) A thick chromium mirror;
(c) A thick platinum mirror.
(d) If the incident x-ray beam is 2 mm high, what length of mirror is required to reflect the entire beam for each material?
5. Calculate the fraction of silver ( Ag ) fluorescence x -rays which are absorbed in a 1 mm thick silicon ( Si ) detector and the charge pulse expected for each absorbed photon. Repeat the calculation for a 1 mm thick germanium ( Ge ) detector.

## Thin plate response - scattering approach

Consider a thin plate of thickness $\Delta$ onto which x-rays are incident from a point source $S$ a perpendicular distance $R_{o}$ away.


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The plate has electron density

$\rho$ and the volume $\Delta d x d y$ contains $\rho \Delta d x d y$ electrons which scatter the $x$-rays.

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$$

## Thin plate response - scattering approach

$R$ is also the distance between the scattering volume and $P$ so, a wave (x-ray) which travels from $S \rightarrow P$ through the scattering volume will have an extra phase shift


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\phi(x, y)=2 k \frac{x^{2}+y^{2}}{2 R_{o}^{2}}=\frac{x^{2}+y^{2}}{R_{o}^{2}} k
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compared to a wave which travels directly along the $z$ axis.

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d \psi_{S}^{P} \approx\left(\frac{e^{i k R_{o}}}{R_{o}}\right)
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$$
d \psi_{S}^{P} \approx\left(\frac{e^{i k R_{o}}}{R_{o}}\right)(\rho \Delta d x d y)
$$

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d \psi_{S}^{P} \approx\left(\frac{e^{i k R_{0}}}{R_{0}}\right)(\rho \Delta d x d y)\left(-b \frac{e^{i k R_{o}}}{R_{o}}\right)
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d \psi_{S}^{P} \approx\left(\frac{e^{i k R_{0}}}{R_{0}}\right)(\rho \Delta d x d y)\left(-b \frac{e^{i k R_{0}}}{R_{0}}\right) e^{i \phi(x, y)}
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d \psi_{S}^{P}=\left(\frac{e^{i k R_{o}}}{R_{o}}\right) \rho(\Delta d x d y)\left(-b \frac{e^{i k R_{o}}}{R_{o}}\right) e^{i \phi(x, y)}
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d \psi_{S}^{P}=\left(\frac{e^{i k R_{o}}}{R_{o}}\right) \rho(\Delta d x d y)\left(-b \frac{e^{i k R_{o}}}{R_{o}}\right) e^{i \phi(x, y)} \quad \begin{aligned}
& \text { Integrate the scattered } \\
& \text { wave over the entire } \\
& \text { plate }
\end{aligned}
$$

## Thin plate response - scattering approach

$$
\begin{gathered}
d \psi_{S}^{P}=\left(\frac{e^{i k R_{o}}}{R_{o}}\right) \rho(\Delta d x d y)\left(-b \frac{e^{i k R_{o}}}{R_{o}}\right) e^{i \phi(x, y)} \\
\psi_{S}^{P}=\int d \psi_{S}^{P}=-\rho b \Delta \frac{e^{i 2 k R_{o}}}{R_{o}^{2}} \int_{-\infty}^{\infty} e^{i \frac{x^{2}+y^{2}}{R_{0}^{2}} k} d x d y
\end{gathered}
$$

Integrate the scattered wave over the entire plate This integral is basically a Gaussian integral with an imaginary (instead of real) constant in the exponent

$$
I^{2}=i \frac{\pi R_{o}}{k}
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& =-\rho b \Delta \frac{e^{i 2 k R_{o}}}{R_{o}^{2}}\left(i \frac{\pi R_{o}}{k}\right)
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## Thin plate response - refraction approach

Now let's look at this phenomenon from a different point of view, that of refraction.


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The phase shift depends on the thickness and the difference between the index of refraction of the medium and that of vacuum

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\psi^{P}=\psi_{o}^{P} e^{i(n-1) k \Delta}=\psi_{o}^{P}[1+i(n-1) k \Delta+\cdots] \approx \psi_{o}^{P}[1+i(n-1) k \Delta]
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## Calculating $n$

We can now compare the expressions obtained by the scattering and refraction approaches.

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Scattering<br>Refraction

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Refraction

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\begin{array}{cc}
\text { Scattering } & \text { Refraction } \\
\psi^{P}=\psi_{o}^{P}\left[1-i \frac{2 \pi \rho b \Delta}{k}\right] & \psi^{P}=\psi_{o}^{P}[1+i(n-1) k \Delta]
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(n-1) k \Delta=-\frac{2 \pi \rho b \Delta}{k}
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$$
\begin{aligned}
(n-1) k \Delta & =-\frac{2 \pi \rho b \Delta}{k} \\
n-1 & =-\frac{2 \pi \rho b}{k^{2}}
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\begin{aligned}
(n-1) k \Delta & =-\frac{2 \pi \rho b \Delta}{k} \\
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$$
\begin{aligned}
(n-1) k \Delta & =-\frac{2 \pi \rho b \Delta}{k} \\
n-1 & =-\frac{2 \pi \rho b}{k^{2}} \\
n & =1-\frac{2 \pi \rho b}{k^{2}}=1-\delta
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## Index of refraction \& critical angle

Now that we have an expression for the index of refraction, we can examine the consequences and estimate it's magnitude.


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Now that we have an expression for the index of refraction, we can examine the consequences and estimate it's magnitude. Consider an x-ray incident on an interface at angle $\alpha_{1}$ to the surface which is refracted into the medium of index $n_{2}$ at angle $\alpha_{2}$.


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Applying Snell's Law

$$
n_{1} \cos \alpha_{1}=n_{2} \cos \alpha_{2}
$$

## Index of refraction \& critical angle

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Consider an x-ray incident on an interface at angle $\alpha_{1}$ to the surface which is refracted into the medium of index $n_{2}$ at angle $\alpha_{2}$.


Applying Snell's Law, and assuming that the incident medium is air (vacuum).

$$
\begin{aligned}
n_{1} \cos \alpha_{1} & =n_{2} \cos \alpha_{2} \\
\cos \alpha_{1} & =n_{2} \cos \alpha_{2}
\end{aligned}
$$

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Now that we have an expression for the index of refraction, we can examine the consequences and estimate it's magnitude.
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$$
\begin{aligned}
n_{1} \cos \alpha_{1} & =n_{2} \cos \alpha_{2} \\
\cos \alpha_{1} & =n_{2} \cos \alpha_{2} \\
\cos \alpha_{1} & =(1-\delta) \cos \alpha_{2}
\end{aligned}
$$

Applying Snell's Law, and assuming that the incident medium is air (vacuum).
If we now apply the known form of the index of refraction for the medium $\left(n_{2}=1-\delta\right)$.

## Index of refraction \& critical angle

Now that we have an expression for the index of refraction, we can examine the consequences and estimate it's magnitude.
Consider an x-ray incident on an interface at angle $\alpha_{1}$ to the surface which is refracted into the medium of index $n_{2}$ at angle $\alpha_{2}$.


Applying Snell's Law, and assuming that the incident medium is air (vacuum).

If we now apply the known form of the index of refraction for the medium

$$
\begin{aligned}
n_{1} \cos \alpha_{1} & =n_{2} \cos \alpha_{2} \\
\cos \alpha_{1} & =n_{2} \cos \alpha_{2} \\
\cos \alpha_{1} & =(1-\delta) \cos \alpha_{2} \\
\cos \alpha_{c} & =1-\delta
\end{aligned}
$$

$\left(n_{2}=1-\delta\right)$.

When the incident angle becomes small enough, there will be total external reflection

## Estimation of critical angle

$$
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& 1-\delta=1-\frac{\alpha_{c}{ }^{2}}{2}+\cdots \\
& 1-\delta \approx 1-\frac{\alpha_{c}{ }^{2}}{2}
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## Estimation of critical angle

For small angles, the cosine function can expanded to give a simple relation for the critical angle

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$$

## Connection to atomic scattering

So far, we have made the assumption that the charge distribution is uniform. We know that this is not correct, and that usually electron charge distributions are those of the atoms making up the solid.
$\psi^{P}=\psi_{o}^{P}\left[1-i \frac{2 \pi \rho b \Delta}{k}\right]$

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## Absorption term in $n$

Since the actual scattering factor of an atom has anomalous terms, $f(Q)=f^{0}(Q)+f^{\prime}+i f^{\prime \prime}$, we must include an absorption term in the model for the index of refraction.

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\mu & =2 \beta k \rightarrow \beta=\frac{\mu}{2 k}
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In terms of the absorption coefficient, $\mu$, and the atomic crosssection, $\sigma_{a}$

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& =-\frac{k}{4 \pi r_{o}} \sigma_{a}
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## Electromagnetic boundary conditions

Maxwell's equations require that an electromagnetic wave and its derivative be continuous in all directions at any interface. This condition places restrictions on the waves which exist at any interface:


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$$
a_{T} k_{T} \cos \alpha^{\prime}=a_{l} k_{l} \cos \alpha+a_{R} k_{R} \cos \alpha
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a_{T} & =a_{l}+a_{R} \\
a_{T} \overrightarrow{k_{T}} & =a_{l} \overrightarrow{k_{l}}+a_{R} \overrightarrow{k_{R}}
\end{aligned}
$$

$$
\begin{aligned}
a_{T} k_{T} \cos \alpha^{\prime} & =a_{l} k_{l} \cos \alpha+a_{R} k_{R} \cos \alpha \\
-a_{T} k_{T} \sin \alpha^{\prime} & =-a_{l} k_{l} \sin \alpha+a_{R} k_{R} \sin \alpha
\end{aligned}
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## Parallel projection \& Snell's Law

Starting with the equation for the parallel projection of the field on the surface and noting that

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\left|\overrightarrow{k_{R}}\right|=\left|\overrightarrow{k_{l}}\right|=k \quad \text { in vacuum }
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$$
\begin{aligned}
\left|\overrightarrow{k_{R}}\right|=\left|\overrightarrow{k_{1}}\right| & =k & & \text { in vacuum } \\
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Combining with the amplitude equation $a_{T} n k \cos \alpha^{\prime}=a_{l} k \cos \alpha+a_{R} k \cos \alpha$ and cancelling

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a_{T}=a_{l}+a_{R} \quad\left(a_{l}+a_{R}\right) n \cos \alpha^{\prime}=\left(a_{l}+a_{R}\right) \cos \alpha
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$$

$$
\left(a_{I}+a_{R}\right) n \cos \alpha^{\prime}=\left(a_{I}+a_{R}\right) \cos \alpha
$$

This simply results in Snell's Law which for small angles can be expanded.

$$
\begin{aligned}
\cos \alpha & =n \cos \alpha^{\prime} \\
1-\frac{\alpha^{2}}{2} & =(1-\delta+i \beta)\left(1-\frac{\alpha^{\prime 2}}{2}\right)
\end{aligned}
$$

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Recalling that

$$
\alpha_{c}=\sqrt{2 \delta}
$$

$$
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1-\frac{\alpha^{2}}{2} & =(1-\delta+i \beta)\left(1-\frac{\alpha^{\prime 2}}{2}\right) \\
-\alpha^{2} & =-\alpha^{\prime 2}-2 \delta+2 i \beta \\
\alpha^{2} & =\alpha^{\prime 2}+\alpha_{c}^{2}-2 i \beta
\end{aligned}
$$

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& -a_{T} n k \sin \alpha^{\prime}=-\left(a_{l}-a_{R}\right) k \sin \alpha
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\left(a_{l}+a_{R}\right) n \sin \alpha^{\prime} & =\left(a_{l}-a_{R}\right) k \sin \alpha \\
\frac{a_{l}-a_{R}}{a_{l}+a_{R}} & =\frac{n \sin \alpha^{\prime}}{\sin \alpha}
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\left(a_{I}+a_{R}\right) n \sin \alpha^{\prime} & =\left(a_{l}-a_{R}\right) k \sin \alpha \\
\frac{a_{l}-a_{R}}{a_{l}+a_{R}} & =\frac{n \sin \alpha^{\prime}}{\sin \alpha} \approx n \frac{\alpha^{\prime}}{\alpha}
\end{aligned}
$$

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$-a_{T} k_{T} \sin \alpha^{\prime}=-a_{l} k_{l} \sin \alpha+a_{R} k_{R} \sin \alpha$
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\left(a_{l}+a_{R}\right) n \sin \alpha^{\prime}=\left(a_{l}-a_{R}\right) k \sin \alpha
$$

$$
\frac{a_{l}-a_{R}}{a_{I}+a_{R}}=\frac{n \sin \alpha^{\prime}}{\sin \alpha} \approx n \frac{\alpha^{\prime}}{\alpha} \approx \frac{\alpha^{\prime}}{\alpha}
$$

$$
\begin{aligned}
& a_{l} \alpha-a_{R} \alpha=a_{l} \alpha^{\prime}+a_{R} \alpha^{\prime} \\
& a_{l}\left(\alpha-\alpha^{\prime}\right)=a_{R}\left(\alpha+\alpha^{\prime}\right)
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& a_{l}\left(\alpha-\alpha^{\prime}\right)=a_{R}\left(\alpha+\alpha^{\prime}\right) \rightarrow r
\end{aligned}
$$

$$
r=\frac{a_{R}}{a_{l}}=\frac{\alpha-\alpha^{\prime}}{\alpha+\alpha^{\prime}}
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$-a_{T} k_{T} \sin \alpha^{\prime}=-a_{l} k_{l} \sin \alpha+a_{R} k_{R} \sin \alpha$
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$$
\left(a_{l}+a_{R}\right) n \sin \alpha^{\prime}=\left(a_{l}-a_{R}\right) k \sin \alpha
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\frac{a_{l}-a_{R}}{a_{l}+a_{R}}=\frac{n \sin \alpha^{\prime}}{\sin \alpha} \approx n \frac{\alpha^{\prime}}{\alpha} \approx \frac{\alpha^{\prime}}{\alpha}
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& a_{l}\left(\alpha-\alpha^{\prime}\right)=a_{R}\left(\alpha+\alpha^{\prime}\right) \rightarrow r \\
& a_{l}\left(\alpha-\alpha^{\prime}\right)=\left(a_{T}-a_{l}\right)\left(\alpha+\alpha^{\prime}\right)
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\end{aligned}
$$

$$
r=\frac{a_{R}}{a_{l}}=\frac{\alpha-\alpha^{\prime}}{\alpha+\alpha^{\prime}} \quad t=\frac{a_{T}}{a_{l}}=\frac{2 \alpha}{\alpha+\alpha^{\prime}}
$$

## Reflectivity and transmittivity

$r$ and $t$ are called the reflection and transmission coefficients, respectively.

$$
\begin{aligned}
& r=\frac{a_{R}}{a_{l}}=\frac{\alpha-\alpha^{\prime}}{\alpha+\alpha^{\prime}} \\
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$r$ and $t$ are called the reflection and transmission coefficients, respectively. The reflectivity $R=\left|r^{2}\right|$ and transmittivity $T=\left|t^{2}\right|$ are the squares of these quantities, which are complex because $\alpha^{\prime}$ is complex.

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\alpha^{\prime}=\operatorname{Re}\left(\alpha^{\prime}\right)+\mathrm{i} \operatorname{Im}\left(\alpha^{\prime}\right)
$$

$$
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\alpha^{\prime}=\operatorname{Re}\left(\alpha^{\prime}\right)+\mathrm{i} \operatorname{Im}\left(\alpha^{\prime}\right)
$$

$$
a_{T} e^{i k \alpha^{\prime} z}=a_{T} e^{i k \operatorname{Re}\left(\alpha^{\prime}\right) z} e^{-k \operatorname{lm}\left(\alpha^{\prime}\right) z}
$$

$$
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$$

$$
a_{T} e^{i k \alpha^{\prime} z}=a_{T} e^{i k \operatorname{Re}\left(\alpha^{\prime}\right) z} e^{-k \ln \left(\alpha^{\prime}\right) z}
$$

$$
\begin{aligned}
& r=\frac{a_{R}}{a_{l}}=\frac{\alpha-\alpha^{\prime}}{\alpha+\alpha^{\prime}} \\
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\end{aligned}
$$

In the $z$ direction, the amplitude of the transmitted wave has two terms with the second one being the attenuation of the wave in the medium due to absorption.

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$$

$$
\Lambda=\frac{1}{2 k \operatorname{lm}\left(\alpha^{\prime}\right)}
$$

$$
\begin{aligned}
& r=\frac{a_{R}}{a_{l}}=\frac{\alpha-\alpha^{\prime}}{\alpha+\alpha^{\prime}} \\
& t=\frac{a_{T}}{a_{l}}=\frac{2 \alpha}{\alpha+\alpha^{\prime}}
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$$

In the $z$ direction, the amplitude of the transmitted wave has two terms with the second one being the attenuation of the wave in the medium due to absorption. This attenuation is characterized by a quantity called the penetration depth, $\Lambda$.

## Wavevector Transfers

While it is physically easier to think of angles, a more useful parameter is called the wavevector transfer.

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$$

in dimensionless units, these become

$$
q=\frac{Q}{Q_{c}} \approx \frac{2 k}{Q_{c}} \alpha \quad q^{\prime}=\frac{Q^{\prime}}{Q_{c}} \approx \frac{2 k}{Q_{c}} \alpha^{\prime}
$$

$q$ is a convenient parameter to use because it is a combination of two parameters which are often varied in experiments, the angle of incidence $\alpha$ and the wavenumber (energy) of the $x$-ray, $k$.

## Defining Equations in $q$

Start with the reduced version of Snell's Law

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\alpha^{2}=\alpha^{\prime 2}+\alpha_{c}^{2}-2 i \beta
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\alpha^{2}=\alpha^{\prime 2}+\alpha_{c}^{2}-2 i \beta
$$

$$
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## Limiting Cases $-q \gg 1$

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$$

$$
q^{\prime 2}=q^{2}\left(1+i \frac{\operatorname{Im}\left(q^{\prime}\right)}{q}\right)^{2}
$$

## Limiting Cases $-q \gg 1$

When $q>1$ "Snell's Law" becomes
we have that $\operatorname{Re}\left(q^{\prime}\right) \approx q$ while the imaginary part can be computed as

$$
\begin{gathered}
q^{2}=q^{\prime 2}+1-2 i b_{\mu} \\
q^{2} \approx q^{\prime 2}-2 i b_{\mu} \\
q^{\prime 2} \approx q^{2}+2 i b_{\mu}
\end{gathered}
$$

$$
\begin{aligned}
q^{\prime} & =q+i \operatorname{Im}\left(q^{\prime}\right) \\
q^{\prime 2} & =q^{2}\left(1+i \frac{\operatorname{Im}\left(q^{\prime}\right)}{q}\right)^{2} \\
& \approx q^{2}\left(1+2 i \frac{\operatorname{Im}\left(q^{\prime}\right)}{q}\right)
\end{aligned}
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& \approx q^{2}+2 i q \operatorname{Im}\left(q^{\prime}\right) \\
\operatorname{Im}\left(q^{\prime}\right) q & \approx b_{\mu} \rightarrow \operatorname{Im}\left(q^{\prime}\right) \approx \frac{b_{\mu}}{q}
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The reflection and transmission coefficients are thus

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reflected wave in phase with incident, almost total transmission

## Limiting Cases - $q \ll 1$

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## Limiting Cases $-q \ll 1$

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q^{\prime 2} & \approx-1
\end{aligned}
$$

## Limiting Cases $-q \ll 1$

When $q \ll 1, q^{\prime}$ is mostly imagi-

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\end{aligned}
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& t=\frac{2 q}{q+q^{\prime}} \approx-2 i q \ll 1
\end{aligned}
$$

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& t=\frac{2 q}{q+q^{\prime}} \approx-2 i q \ll 1 \\
& \Lambda \approx \frac{1}{Q_{c}}
\end{aligned}
$$

## Limiting Cases $-q \ll 1$

When $q \ll 1, q^{\prime}$ is mostly imaginary with magnitude 1

$$
\begin{aligned}
q^{2} & =q^{\prime 2}+1-2 i b_{\mu} \\
q^{\prime 2} & \approx-1 \\
q^{\prime} & \approx i
\end{aligned}
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Thus the reflection and transmission coefficients become

$$
\begin{aligned}
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& t=\frac{2 q}{q+q^{\prime}} \approx-2 i q \ll 1 \\
& \Lambda \approx \frac{1}{Q_{c}}
\end{aligned}
$$

The reflected wave is out of phase with the incident wave, there is only small transmission in the form of an evanescent wave, and the penetration depth is very short.

## Limiting Cases - $q \sim 1$

If $q \sim 1$

$$
q^{2}=q^{\prime 2}+1-2 i b_{\mu}
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& q^{2}=q^{\prime 2}+1-2 i b_{\mu} \\
& q^{\prime 2} \approx 2 i b_{\mu}=b_{\mu}(2+2 i-2)
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q^{2} & =q^{\prime 2}+1-2 i b_{\mu} \\
q^{\prime 2} & \approx 2 i b_{\mu}=b_{\mu}(2+2 i-2) \\
& =b_{\mu}(1+i)^{2}
\end{aligned}
$$

## Limiting Cases - $q \sim 1$

If $q \sim 1, q^{\prime}$ is complex with real and imaginary parts of equal magnitude.

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\begin{aligned}
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The reflected wave is in phase with the incident, there is significant (larger amplitude than the reflection) transmission with a large penetration depth.

